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3
PHOTOGRAMMETRIC METHODS FOR MEASUREMENTS IN FLUID PHYSICS
EXPERIMENTS IN SPACE†

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15 **Abstract**—Methods of digital close-range photogrammetry allow for manifold real 3-D measure-
17 ments in dynamic processes. Based on the acquisition of multi-camera digital image sequences, im-
19 age analysis with subpixel accuracy image measurement operators, photogrammetric multi-image
21 matching and point determination techniques, strict geometric modeling of complex environments
23 and thorough system calibration techniques, time-resolved accurate 3-D coordinates of a large num-
25 ber of objects in a scene can be determined fully automatically. The paper will first give a short
27 review on basic principles of digital photogrammetry and discuss the application and accuracy po-
tential. After that, practical examples will be given from several breadboard experiments conducted
in the frame of the ESA Technological Research and Development Programme to show the applica-
bility of the technique to typical experiments in the field of fluid physics. These experiments focus
on the investigation of experiments on Marangoni convection; they include the determination of
3-D velocity fields near a hanging drop within a fluid matrix and the observation of the tangential
tension on the boundary surface by measuring changes in shape and/or position of liquid bodies
like drops, bubbles or liquid columns in a fluid matrix. © 2001 Published by Elsevier Science Ltd.

29 1. INTRODUCTION

31 Compared to Earth's environment, microgravity is
33 a challenging chance offered, to basic science for
35 achieving a deeper understanding of fundamental
37 physical phenomena, and to technology for im-
39 proving several technologically oriented processes.
The investigation of liquid flows due to thermal
gradients in a fluid matrix is of great importance
in the study of heat and mass transfer processes,
for both fundamental research and technology.

41 One example is the analysis of thermocapillary
43 flows: While on Earth the thermocapillary ef-
45 fect is covered by buoyancy, in microgravity it
47 can play a leading role. From the industrial point
49 of view, several processes can benefit from the
51 buoyancy-absent Space environment: Material
53 production processes and solidification front dy-
55 namics can be improved, leading to products of
higher quality than those produced on Earth.

To be able to analyze fluid physics phenomena
quantitatively, measurement techniques have to
be applied with the aim of determining shape and
motion parameters. Due to the three-dimensional
dynamic character of many phenomena, these mea-
surements should preferentially cover the whole
experimental volume at once. Methods of digital

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1 photogrammetry offer themselves for such tasks,
 2 as they allow for the determination of accurate
 3 three-dimensional information simultaneously at
 4 many locations of an observation volume in a
 5 non-contact manner and without the risk of distur-
 6 bances as created by mechanically driven scanning
 7 devices.

8 To be able to judge the potential of digital pho-
 9 togrammetric techniques in the field of fluid physics
 10 measurements, two studies were performed on pho-
 11 togrammetric methods applied to fluid motion visu-
 12 alized by tracers and on liquid bodies. In the course
 13 of the studies, breadboards were developed for two
 14 experiments: In an experiment on thermocapillary
 15 convection in a liquid around a gas bubble, 3-D
 16 velocity vectors and trajectories of several hundred
 17 flow markers were determined simultaneously using
 18 a four-camera imaging system. Another bread-
 19 board was built for the measurement of position
 20 and shape of liquid bodies as a function of time. In-
 21 vestigations concentrated on the development of a
 22 compact and exchangeable multi-camera observa-
 23 tion module and an imaging chain for the data flow
 24 concerning photogrammetric measurements on mi-
 25 crogravity experiments.

2. DIGITAL PHOTOGRAMMETRY

27 With the development of solid state sensor imag-
 28 ing devices and powerful computer platforms, new
 29 image-processing-based solutions for a large num-
 30 ber of 3-D measurement tasks have become possi-
 31 ble in the past two decades. While computer vision
 32 does often deal with more qualitative image un-
 33 derstanding tasks and machine vision is mainly to
 34 be seen in the context of industrial production line
 35 applications, digital photogrammetry aims at the
 36 derivation of accurate 3-D metric information from
 37 multiple digital images.

38 Besides subpixel accuracy image measure-
 39 ment operators, strict geometric modeling and a
 40 thorough system calibration provide the basis to
 41 achieve high accuracies in 3-D space with vision
 42 systems based on off-the-shelf vision hardware
 43 components. The basic equation of photogrammet-
 44 ric 3-D coordinate determination is the collinearity
 45 equation (see e.g. [1]) which simply states that
 46 object point, camera projective center and image
 47 point lie on a straight line. This mathematical
 48 formulation has to be extended to meet the physi-
 49 cal realities. Effects caused by lens distortion and
 50 A/D conversion are usually compensated by a set
 51 of additional parameters, which have to be deter-
 52 mined in the system calibration together with the
 53 parameters of exterior and interior orientation of

the cameras. Lens distortion is often compensated
 54 by a set of five additional parameters modeling
 55 radial and decentering distortion [2]. For the com-
 56 pensation of electronic effects, especially the often
 57 a priori unknown difference between the pixel rate
 58 of a camera and the clock rate of a framegrabber,
 59 an additional transformation with two parameters
 60 of an affine transformation [3] is often adjoined.
 61 These parameters have to be determined in a sys-
 62 tem calibration before, during or after the image
 63 acquisition of an actual measurement task. The
 64 most flexible way of determining these system pa-
 65 rameters is self-calibrating bundle adjustment [4],
 66 in which 3-D object coordinates, camera orienta-
 67 tion data and camera calibration parameters are
 68 determined simultaneously, based only on image
 69 coordinate measurements and at least one scale
 70 information in object space. To warrant good deter-
 71 minability of all parameters, the acquisition of
 72 multiple images of the scene with each camera un-
 73 der different orientations is required. Besides this,
 74 multiple images are also useful for the improve-
 75 ment of the precision of the object point coordi-
 76 nates and the capability of self-diagnosis (control
 77 of the quality of measurements and results based
 78 on redundant information in the least-squares esti-
 79 mation process). For applications in fluid physics
 80 experiments, the collinearity equation has to be
 81 extended to meet the reality of objects in a liquid
 82 which are imaged through a transparent window,
 83 thus causing multiple twice-broken beams to be
 84 intersected for 3-D object point coordinate deter-
 85 mination. These twice-broken beams can be han-
 86 dled with a strict geometric modeling contained
 87 in a multimedia module [5]. The module also al-
 88 lows for the handling of multiply broken beams as
 89 caused by multi-containments.

90 Due to the nature of digital images, automation is
 91 an inherent characteristic of digital photogrammet-
 92 ric data processing as well as real-time or on-line
 93 processing aspects, thus making it well suited for
 94 dynamic applications. Using standard image acqui-
 95 sition devices like standard videonorm CCD cam-
 96 eras ($\sim 768 \times 576/480$ pixels, 25/30 images/s),
 97 subpixel operators measuring the image coordi-
 98 nates of features with a precision of 1/10–1/50
 99 pixel and appropriate system calibration tech-
 100 niques, relative precisions in the order of 1:20,000
 101 of the object space dimensions can be achieved
 102 in dynamic applications. This potential allows for
 103 the substitution of film-based cameras by solid
 104 state sensor cameras, which has to be considered
 105 an enormous improvement concerning Space in-
 106 strumentation. Quantitative image data will be
 107 available via the communication link, an absolute

prerequisite concerning an intensive use of the International Space Station. With large format solid state cameras and the acquisition of a large number of images of a static object, an accuracy potential of better than 1:100,000 has been achieved. A detailed review of the historical development of digital close range photogrammetry and a number of application examples in different fields is given in [6].

3. THREE-DIMENSIONAL PARTICLE TRACKING VELOCIMETRY

Techniques of digital photogrammetry are suitable for static applications as well as for 3-D measurement tasks in dynamic processes. A typical application field of digital photogrammetric techniques in dynamic processes is 3-D particle tracking velocimetry (PTV). 3-D PTV is based on tracking a large number of discrete flow markers in multi-camera image sequences and depicts a robust and accurate technique, which is capable of delivering truly 3-D velocity field information (i.e. all three vector components in a 3-D observation volume) at a high spatial and a sufficient temporal resolution. It is based on the acquisition and processing of stereoscopic image sequences of moving particles.

Figure 1 shows the data flow of 3-D PTV data processing. The first step in the fully automatic data processing chain is a high-pass filtering of the images in order to eliminate global image contrast and to remove some non-uniformities of the background intensity introduced by effects of the illumination. After that, particles can be detected by thresholding, and their location in image space can be determined with subpixel accuracy by a centroid operator [7].

The most critical step of automatic 3-D PTV data processing is the establishment of stereoscopic correspondences between particle images as a prerequisite for 3-D coordinate determination. Particle features (like size, shape, color) do not usually allow for a reliable distinction between matching candidates, the more so as these features are furthermore influenced by the imaging process. Thus, the only information that can be used for the establishment of correspondences is the geometric information provided by the epipolar line: Knowing the orientation parameters of the cameras from a calibration procedure, the search space for corresponding points can be reduced to a line plus tolerance in image space. However, this search on epipolar lines will produce ambiguities in applications with dense tracer seeding. These ambiguities can be solved by using three or four synchronized

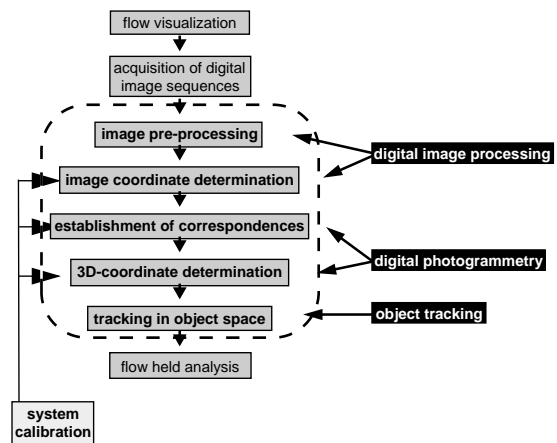


Fig. 1. Dataflow scheme for 3-D PTV data processing.

cameras rather than two and applying trinocular or multiocular vision techniques [7].

In the next processing step the 3-D coordinates of all particles can be determined by spatial intersection, taking into account the beam deflections caused by the glass window on the optical path. The redundant information provided by the measurement of three or four times two image coordinates for the determination of three object space coordinates increases the precision and allows to perform a least-squares adjustment for each individual point, thus providing additional precision estimates.

For a more detailed description of data acquisition system configurations, image processing, establishment of multi-view correspondences, geometric modeling and system calibration see [8].

As less ambiguities can be expected when tracking is performed in 3-D space, the establishment of temporal correspondences is the last step in the processing chain as outlined here. The tracking is based on principles that are rather similar to the treatment of ambiguities during the establishment of multi-image correspondences, solving possible ambiguities by the propagation and verification of possible links between two time instances into a third time instance under assumptions on the maximum Lagrangian acceleration [9].

Using four CCD cameras and an image format of only 512×512 pixels, the method allows for the determination of velocity vectors of more than 1000 particles per time instant. The relative accuracies of the vector components are approximately 1:4000 (standard deviation of X and Y coordinates over field of view) with the accuracy of the depth component Z being typically by a factor of two to three worse than the components perpendicular to the main viewing direction. For a cubic volume of

1 1 l that means 0.025 mm in X and Y directions and
 2 0.060 mm in Z direction; this is compatible with
 3 the requirement for spatial resolution of 0.1 mm
 4 given for the diagnostic tools of the Fluid Science
 5 Laboratory (FSL). These figures are valid under
 6 controlled conditions; suboptimal illumination con-
 7 ditions, complex flows, temperature gradients or
 8 image noise may lead to a severe degradation of the
 9 potential. In addition to the 3-D vector fields, PTV
 10 is also capable of determining long particle trajec-
 11 tories, if storage capacity for image sequences is
 12 available. In practical experiments, particles could
 13 be traced over several hundred frames when the
 14 number of particles in the observation volume was
 15 kept small [10].

16 The unique features of the technique and its
 17 unrivaled suitability for 3-D velocity field
 18 measurements provide a solution to a number
 19 of measurement tasks which could so far not be
 20 realized.

21 4. APPLICATION OF 3-D PTV IN THERMOCAPILLARY 22 CONVECTION EXPERIMENTS

23 To verify the potential of 3-D PTV for the solution
 24 of fluid physics measurement tasks, a breadboard
 25 experiment on the determination of 3-D velocity
 26 fields in the vicinity of a gas bubble (Marangoni
 27 convection) was set up [11]. The experiment setup
 28 is a replica of an experiment described in [12].

29 The mechanism of Marangoni convection is out-
 30 lined in Figs. 2 & 3: At the interface between two
 31 immiscible fluids a curved surface will be generated
 32 by the surface tension. Local variations of this sur-
 33 face tension, caused by temperature gradients, in-
 34 duce a capillary convection parallel to the surface.
 35 The interaction between this surface-tension-driven
 36 convection and gravity-driven convection leads to
 37 a complicated flow field, which is to be examined
 over time in all three dimensions.

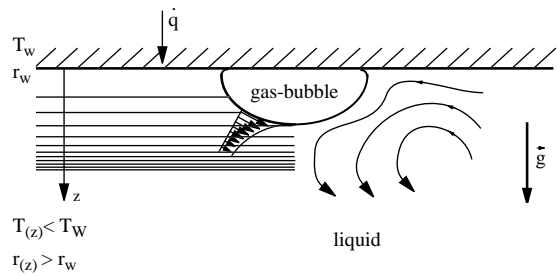


Fig. 3. Mechanism of thermocapillary convection in the surrounding of a bubble under a heated horizontal wall.

39 To generate and observe Marangoni convection
 40 effects around a gas bubble in silicon oil, a top
 41 heated fluid cell has been designed and constructed
 42 similar to the one described in [12]. It consists of
 43 a cubic cell with inner dimensions of $90 \times 90 \times$
 44 90 mm^3 and glass walls for optical access of a pho-
 45 togrammetric multi-camera module and a tracer il-
 46 lumination device. Top and bottom plates are de-
 47 signed for heating and cooling, fluid supply and
 48 drainage; they contain several temperature probes
 49 and facilities for the generation and adjustment of
 50 a gas bubble. The liquid in the cell is seeded with
 51 neutrally buoyant tracer particles, which are suit-
 52 ably illuminated and imaged by a system consisting
 53 of four CCD cameras (Fig. 4).

54 The observation system was calibrated before
 55 and/or after an experiment by imaging a 3-D
 56 reference body covering the observation volume
 57 with a large number of targets with known co-
 58 ordinates. This calibration procedure using 3-D
 59 reference avoids the necessity of the acquisition of
 60 multiple images with each camera as required by
 61 self-calibration techniques; it allows for the deter-
 62 mination of the parameters of camera orientation
 63 as well as parameters describing the camera model,
 64 lens distortion and other disturbances. Using the
 65

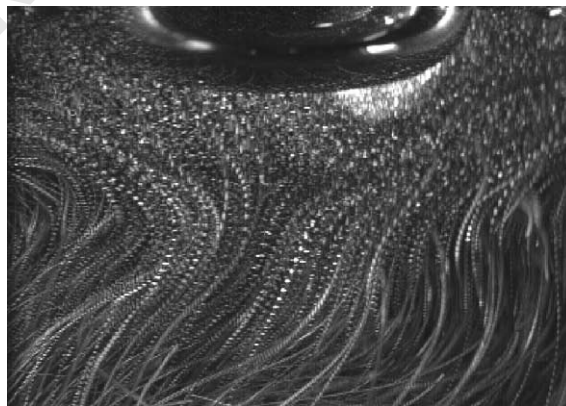


Fig. 2. Section of an accumulated particle image (Marangoni convection experiment).



Fig. 4. Four-camera 3-D PTV arrangement, fluid cell with calibration body.

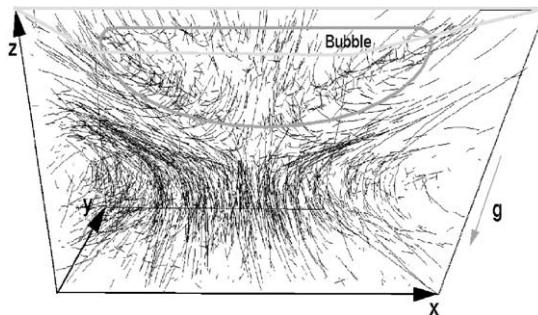


Fig. 5. 8000 out of 100,000 3-D velocity vectors in sub-volume of $10 \times 8 \times 6 \text{ mm}^3$ of a Marangoni convection experiment ($\text{Ma} = 600$), recorded at 400 time steps over 20 min.

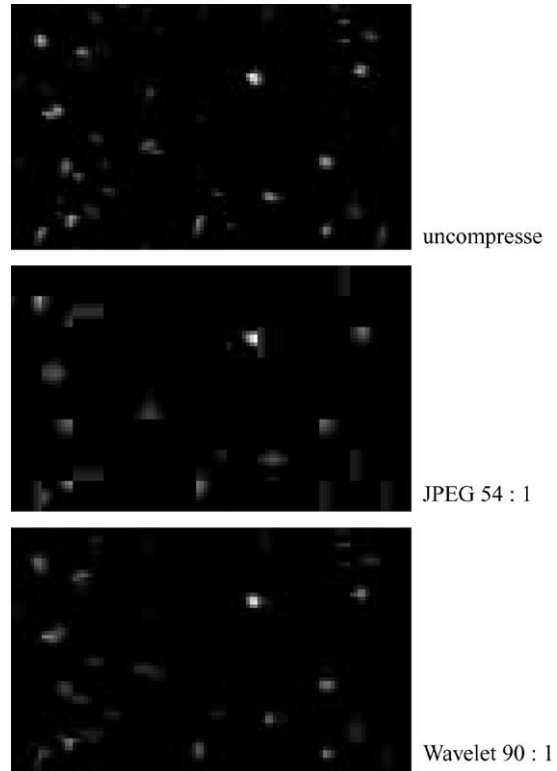


Fig. 6. Effects of high compression ratios to particle images (104×80 pixel image region).

1 calibration parameters and the data processing
 3 chain as outlined in Fig. 1, 200–500 velocity vec-
 5 tors per time instant could be determined in an
 7 observation volume of $20 \times 14 \times 14 \text{ mm}^3$ centered
 9 around the gas bubble. A sample of a velocity field
 11 is shown in Fig. 5.

7 The precision of the velocity vector components
 9 within the observation volume was estimated to be
 11 in the order of $5\text{--}10 \mu\text{m}$ for the two lateral compo-
 13 nents (X, Z) and $20\text{--}30 \mu\text{m}$ for the component in
 15 camera viewing direction (Y).

13 The high data rate of techniques based on image
 15 sequence processing poses severe requirements to
 17 data storage systems. if data cannot be processed in
 19 real time. As an option to reduce the amount of data
 21 to be stored intermediately, advanced transform
 23 coding based compression algorithms for lossy image
 25 compression were quantitatively examined in order
 to be able to evaluate the ability of different
 algorithms to preserve the image information
 which is relevant for the photogrammetric applica-
 tion when high compression factors are required.
 In particular, the Discrete Cosine Transform based
 JPEG standard and the Discrete Wavelet Transform
 based EZW scheme were examined. The results indicate
 that for particle images a compression factor

of 10–15 can be achieved at an acceptable loss of
 data quality, leading to a proportional reduction of
 data transmission bandwidth requirements and ex-
 tension of recording time.

For these compression ratios no significant
 difference could be detected between JPEG and
 wavelets. As much higher compression factors (90
 –120) have to be applied for telepresence purposes,
 the influence of the two compression techniques
 was also tested at those qualitative images. Here
 JPEG fails and leads to unacceptable blocking
 effects, while images compressed/decompressed
 with the wavelet-based technique still show details
 of the convective currents, which is a must for
 telepresence (Fig. 6).

The study has shown that the advantages of 3-D
 PTV as a non-invasive, simultaneous, accurate,
 unbiased, truly three-dimensional technique for
 the determination of a large number of velocity
 vectors and trajectories in combination with strict
 geometric and statistical modeling including the
 capability of determining the precision of the deliv-
 ered information and detecting deviations from
 the mathematical or the statistical model qualify
 the technique for the use in complex flow mea-
 surement applications.

1 On the basis of the promising results gained
 3 through the investigation of thermocapillary con-
 5 vective flows around a hanging drop in a fluid ma-
 7 trix using 3-D PTV, another project is currently in
 progress, whose aim is to determine, presently on
 Earth, velocity fields in smaller and more complex
 fluid volumes, like liquid bridges under mechanical
 and thermal stress.

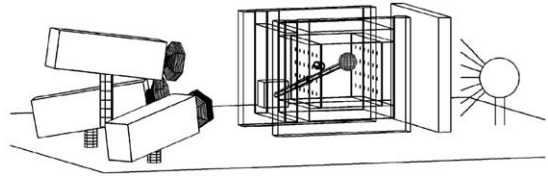


Fig. 7. Breadboard for liquid body measurement.

9 5. EXPERIMENT ON MEASUREMENT OF POSITION AND SHAPE OF LIQUID BODIES

11 For the observation of tangential tension on the
 13 boundary surface between two media it is neces-
 15 sary to determine the velocity of liquid bodies, e.g.
 17 drops and columns, within a fluid matrix and/or
 their change of shape in time. To demonstrate the
 performance of photogrammetric methods concern-
 ing the study of those phenomena, a demonstration
 breadboard of a photogrammetric diagnostic tool
 has been developed and built [13].

21 This breadboard developed for ESA/ESTEC
 [14] consists of the fluid cell, a motion device, the
 23 drop and column dummies and the photogram-
 metric front end. The photogrammetric front end
 consists of three CCD cameras, which form a
 25 compact setup in front of one observation window
 of the fluid cell, and facilities for the calibration
 27 of this photogrammetric measuring unit (Fig. 7).

29 The dimension of the fluid cell and the fluid body
 chosen are representative of typical microgravity
 experiments [15]. The objects can be moved within
 31 the fluid cell with an inner size of $50 \times 50 \times 70 \text{ mm}^3$.
 A double-walled window has been chosen to rep-
 33 resent the thermal insulation of a typical cell, and
 a window thickness of 10 mm is representative in
 35 case interferometric methods are also applied. A
 reseau grid is placed on the inner sides of the front
 37 and back windows of the fluid cell. Top and bot-
 39 tom windows are also made of glass to be able
 to use additional observation techniques. The ob-
 41 jects are inserted into a silicone oil fluid matrix.
 The drop and the fluid column dummies represent-
 43 ing the model scene are manufactured from solid
 transparent materials. To simulate different sizes of
 45 the drops high-precision glass balls with diameters
 from 2 to 20 mm can be attached to a moveable rod;
 47 to simulate the column bodies three different ob-
 jects with cylindrical, spheroidal and hyperboloidal
 49 shape are manufactured from Plexiglas and can be
 mounted instead.

51 The three cameras of the photogrammetric ob-
 53 servation module are fixed on a common frame
 with their relative positions chosen with respect to
 the size of the observation window and the depth

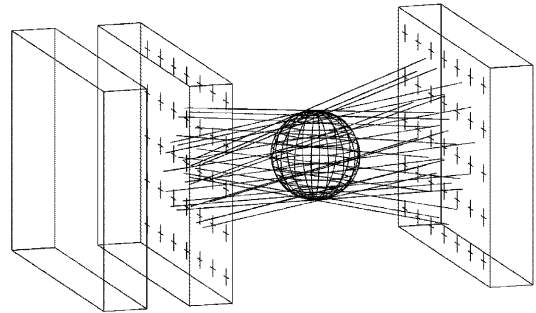


Fig. 8. Tangent lines between reseau planes.

of the scene to be observed. Such a photogram-
 metric observation module can be used for measure-
 55 ments on different types of experiments. It can be
 exchanged with other diagnostic tools and because
 57 it is applied from one side only it can even be used
 simultaneously with other diagnostic tools like in-
 59 terferometry for example.

61 Instead of the fluid cell, a testfield can be
 mounted in front of the measuring head for a pre-
 63 cise automatic calibration of the camera setup.
 This concept of exchangeable, reconfigurable mea-
 65 suring heads together with exchangeable experi-
 ment cells gives highest flexibility concerning the
 67 different types of experiments to be expected.

69 The calibration of the camera head can be per-
 formed prior to the actual measurement with a test-
 71 field calibration procedure [16]. Instead of a strict
 geometric modeling of the optical path, correction
 73 parameters due the multi-media path can be calcu-
 lated by observing a grid of reseau crosses on the
 75 inner sides of the front and back observation win-
 dows and comparing to the known grid mesh val-
 77 ues. This way even local deviations of the refractive
 index in the fluid due to temperature gradients can
 79 be corrected. This calibration of the multi-media
 path can be performed before the actual image se-
 81 quence in a thermally balanced state of the experi-
 ment or on-line at each step of the image sequence.

83 For the reconstruction of the liquid bodies the
 85 edges are measured with subpixel accuracy in the
 digital images. The connections of the interpolated
 edge points in the two reseau planes form tangents
 lines to the liquid bodies (Fig. 8). The evaluation

1 procedure for the liquid bodies is a least-squares
2 adjustment with the tangent lines as observations
3 and different basic distance functions describing the
4 liquid bodies as unknown parameters.

5 Results of the evaluation of typical bubble se-
6 quences and column movements showed accura-
7 cies of the position and shape of the liquid bodies
8 in the order of 20–30 μm .

9 In a second part of the study work will focus
10 on the measurement of shape changes of arbitrarily
11 shaped liquid columns and the investigation of the
12 influence of different compression techniques on
13 the measurement results.

6. CONCLUSION

15 The results of the breadboard experiments,
16 achieved with relatively compact, stable and eco-
17 nomic measurement systems, show the suitability
18 of photogrammetric techniques for applications in
19 fluid physics experiments in space. Although the
20 breadboards were primarily designed for labora-
21 tory use, much effort was made to design the pho-
22 togrammetric observation modules with respect
23 to the specific needs of fluid physics experiments
24 under microgravity conditions onboard a Space
25 station.

26 Beyond the experiments performed within the
27 studies, the technology of melt processes and crys-
28 tal growth could also benefit from these achieve-
29 ments. If it is demonstrated that also very complex
30 flow phenomena, like oscillating liquid bridges, can
31 be analyzed through photogrammetric techniques,
32 as for both the velocity field of tracers inside the
33 column and the changing shape of the column it-
34 self, this optical method will have a good chance
35 to become a multi-user diagnostic tool, simplifying
36 Space facilities.

7. UNCITED REFERENCE

[17]

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