

Rotations & Articulated Objects

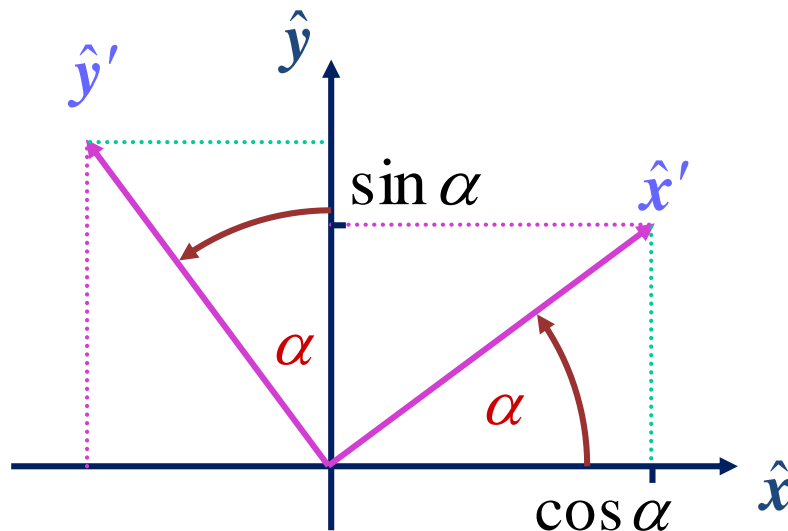


- ◆ 2D rotations
- ◆ 3D rotations
- ◆ Quaternions
- ◆ Articulated Objects



2D ROTATIONS

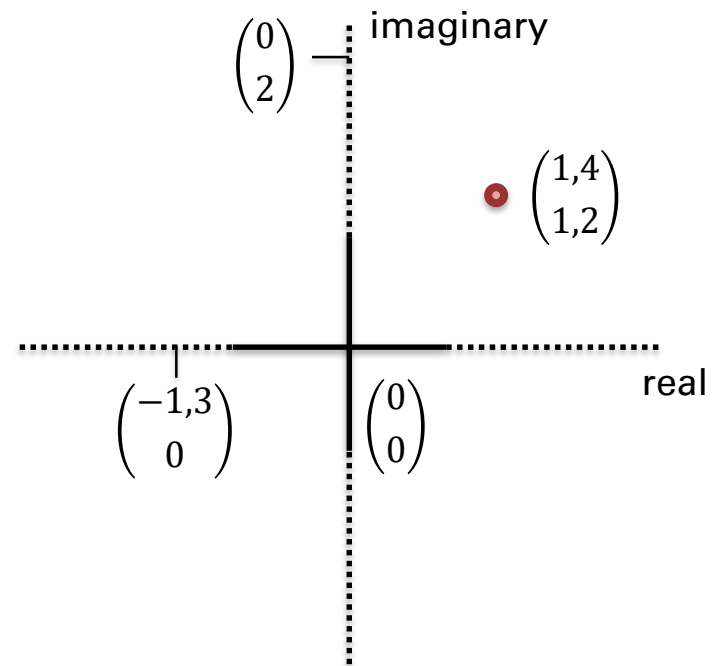
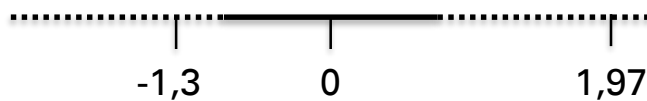
- Transformation matrices contain the new base vectors in their columns (or rows, depending on the convention)
- For example: counter clockwise rotation around angle α



$$M = \begin{pmatrix} \cos \alpha & -\sin \alpha \\ \sin \alpha & \cos \alpha \end{pmatrix}$$

Complex Numbers

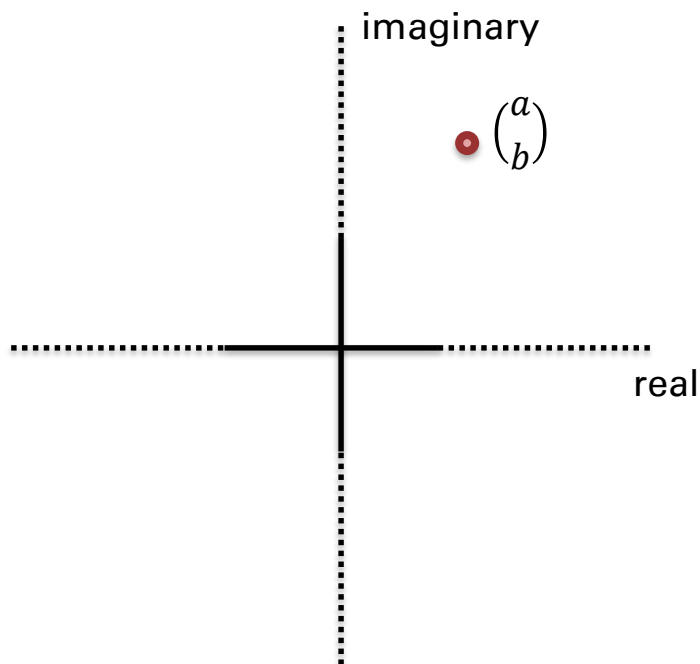
- ◆ The equation $x^2+1=0$ has no solution in \mathbf{R}
- ◆ With the definition $i = \sqrt{-1}$ we get the solutions $x=\pm i$
- ◆ Besides the “real” dimension, an imaginary dimension extends the 1d real space to the 2d complex space
- ◆ By definition, the real dimension and the imaginary dimension are orthogonal



- ◆ Different equivalent notions exist to describe a point in the complex plane

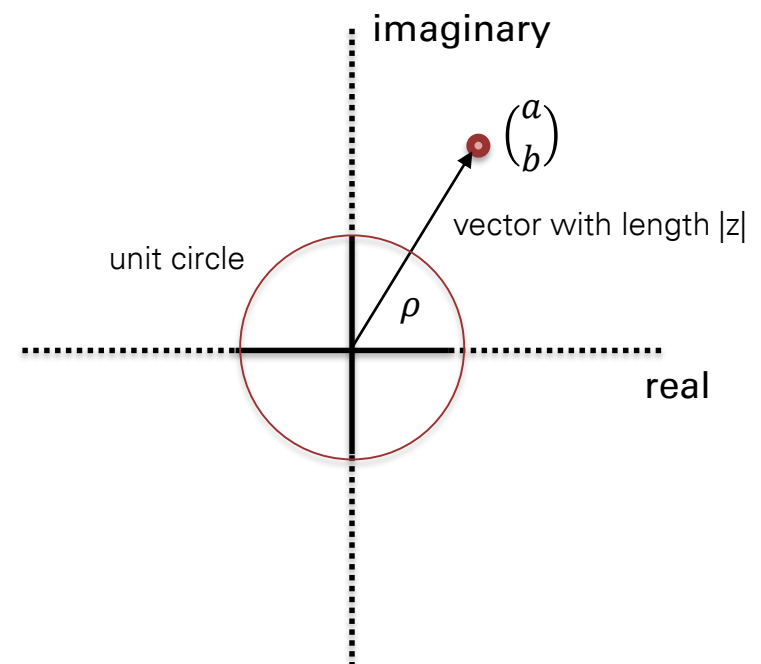
component form

$$z = a + i \cdot b$$



trigonometric form

$$z = |z| \cdot (\cos \rho + i \cdot \sin \rho)$$





- ◆ product is defined by distribution law and the basic products $1 \cdot 1 = 1$, $1 \cdot i = i$, $i \cdot 1 = i$, $i \cdot i = -1$:

$$(a + ib)(c + id) = ac - bd + i(bc + ad)$$

- ◆ complex product is commutative:

$$z_1 \cdot z_2 = z_2 \cdot z_1$$

- ◆ conjugation: $z^* = (a + ib)^* = a - ib$

- ◆ norm: $|z|^2 = z \cdot z^* = a^2 + b^2$

- ◆ inverse: $z^{-1} = z^* / |z|^2$

- ◆ any polynomial $\sum_{j=0 \dots n} a_j \cdot x^j$ has n zero crossings in \mathbb{C}



Euler's Formula

- ◆ Euler published in 1748 the formula

$$\exp(i \cdot \rho) = \cos \rho + i \cdot \sin \rho$$

that shows $\exp(i \cdot \rho)$ repeatedly traces out the unit circle.

- ◆ The proof is given by Taylor series expansions:

$$\exp(x) = 1 + x + \frac{1}{2}x^2 + \frac{1}{6}x^3 + \frac{1}{24}x^4 + \frac{1}{120}x^5 + \dots$$

- ◆ plugging in $x = i\alpha$ yields

$$\begin{aligned}\exp(i\alpha) &= 1 + i\alpha - \frac{1}{2}\alpha^2 - i\frac{1}{6}\alpha^3 + \frac{1}{24}\alpha^4 + i\frac{1}{120}\alpha^5 + \dots \\ &= 1 - \frac{1}{2}\alpha^2 + \frac{1}{24}\alpha^4 + \dots + i\left(\alpha - \frac{1}{6}\alpha^3 + \frac{1}{120}\alpha^5 + \dots\right) \\ &= \cos \alpha + i \cdot \sin \alpha\end{aligned}$$

- ◆ the trigonometric form of a complex number becomes

$$z = |z| \cdot \exp(i\rho) = |z| \cdot e^{i\rho}$$

2D Rotation with complex numbers



- multiplication of a complex number $z = a + ib$ from **left** or **right** with $e^{i\alpha}$ corresponds to 2D rotation of z around origin in complex plane
- proof by reduction to matrix form:

$$\begin{aligned} z \cdot e^{i\alpha} &= (a + ib) \cdot e^{i\alpha} \\ &= (a + ib) \cdot (\cos \alpha + i \cdot \sin \alpha) \\ &= a \cdot \cos \alpha + i \cdot a \cdot \sin \alpha + i \cdot b \cdot \cos \alpha - b \cdot \sin \alpha \\ &= a \cdot \cos \alpha - b \cdot \sin \alpha + i \cdot (a \cdot \sin \alpha + b \cdot \cos \alpha) \\ &= \begin{pmatrix} \cos \alpha & -\sin \alpha \\ \sin \alpha & \cos \alpha \end{pmatrix} \begin{pmatrix} a \\ b \end{pmatrix} \\ &= (\cos \alpha + i \cdot \sin \alpha) \cdot (a + ib) \\ &= e^{i\alpha} \cdot z \end{aligned}$$



3D ROTATIONS

Properties of rotations in 3D

- Rotations retain the length of vectors, which means

$$\begin{aligned} \langle \vec{v}, \vec{v} \rangle &= \langle R\vec{v}, R\vec{v} \rangle \\ &= (R\vec{v})^T R\vec{v} \\ &= \vec{v}^T R^T R\vec{v} \end{aligned}$$

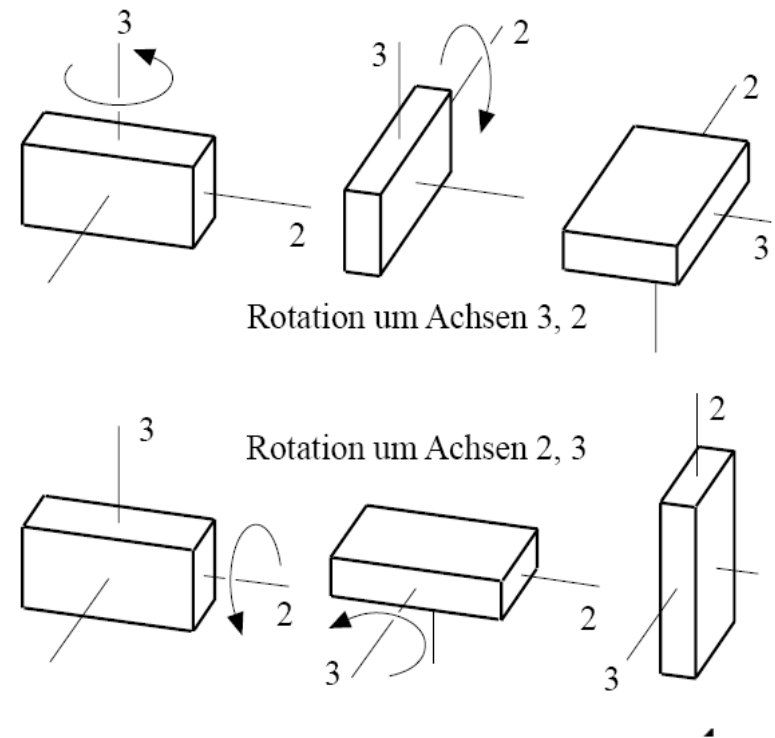
- This is true for all \vec{v} , thus

$$\begin{aligned} R^T R &= I \quad \Rightarrow \quad R^{-1} = R^T \\ &\Rightarrow \quad \det R = \pm 1 \end{aligned}$$

- If $\det R = -1$ the matrix contains a reflection. Rotations must have $\det R = +1$
- Rotations form the special orthonormal group:

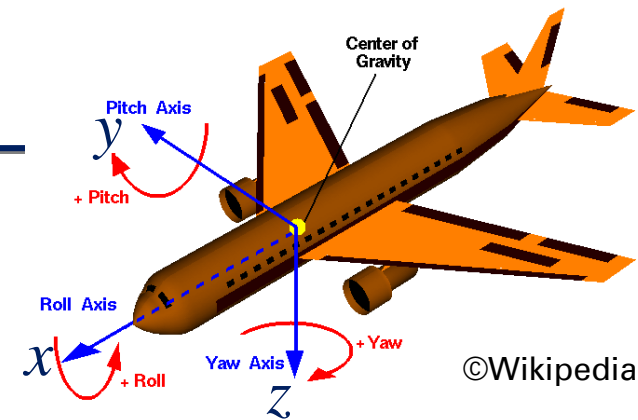
$$\forall R_1, R_2 \in SO(3) : R_1 R_2 \in SO(3)$$

- 3D rotations do not commute:



Forward Euler Angle

- A 3D rotation in the 123-convention of Euler angles as used in navigation for roll, pitch, yaw can be written in the form:



$$R_x(\theta_1) R_y(\theta_2) R_z(\theta_3) = \begin{pmatrix} 1 & 0 & 0 \\ 0 & c_1 & s_1 \\ 0 & -s_1 & c_1 \end{pmatrix} \begin{pmatrix} c_2 & 0 & -s_2 \\ 0 & 1 & 0 \\ s_2 & 0 & c_2 \end{pmatrix} \begin{pmatrix} c_3 & s_3 & 0 \\ -s_3 & c_3 & 0 \\ 0 & 0 & 1 \end{pmatrix}$$

$$= \begin{pmatrix} c_2 c_3 & c_2 s_3 & -s_2 \\ s_1 s_2 c_3 - c_1 s_3 & s_1 s_2 s_3 + c_1 c_3 & s_1 c_2 \\ c_1 s_2 c_3 + s_1 s_3 & c_1 s_2 s_3 - s_1 c_3 & c_1 c_2 \end{pmatrix}$$

with $c_1 = \cos \theta_1$, $s_1 = \sin \theta_1$, etc.

- The Euler angles can be computed from a given rotation matrix \mathbf{R} according to the Pseudo code on next slide. We define the vector $\vec{\omega}$ of Euler angles as

$$\vec{\omega} = (\theta_1, \theta_2, \theta_3)^T = R_{123}^{-1}(\mathbf{R})$$

Euler Angles Inversion – 2 Approaches



$$M = \begin{pmatrix} m_{00} & m_{01} & m_{02} \\ m_{10} & m_{11} & m_{12} \\ m_{20} & m_{21} & m_{22} \end{pmatrix} = \begin{pmatrix} c_2 c_3 & c_2 s_3 & -s_2 \\ s_1 s_2 c_3 - c_1 s_3 & s_1 s_2 s_3 + c_1 c_3 & s_1 c_2 \\ c_1 s_2 c_3 + s_1 s_3 & c_1 s_2 s_3 - s_1 c_3 & c_1 c_2 \end{pmatrix}$$

Ken Shoemake. "Euler angle conversion." Graphics gems IV. 1994. 222-229.

- checks for gimble lock case where c_2 becomes very small with epsilon check on m_{00} and m_{01} and assumes $\theta_3 = 0$.

- Mike Day. "[Extracting euler angles from a rotation matrix](#)", 2012

- avoids check by accounting for instable θ_1 in computation of θ_3
- this allows for restriction to single precision floats

$$\theta_1 = \text{atan2}(m_{12}, m_{22})$$

$$c_2 = \sqrt{m_{00}^2 + m_{01}^2}$$

$$\theta_2 = \text{atan2}(-m_{02}, c_2)$$

$$\theta_3 = \text{atan2}(m_{01}, m_{00})$$

$$= \text{atan2}(c_2 s_3, c_2 c_3)$$

$$s_1 = \sin(\theta_1), \quad c_1 = \cos(\theta_1)$$

$$\theta_3 = \text{atan2}(s_1 m_{20} - c_1 m_{10}, c_1 m_{11} - s_1 m_{21})$$

Rotation around Axis

- Every rotation can be described by an axis \hat{n} and an angle α
- Notion of this rotation matrix $\mathbf{R}(\hat{n}, \alpha)$
- For every rotation exist two axis-angle combinations:

$$\mathbf{R}(\hat{n}, \alpha) = \mathbf{R}(-\hat{n}, -\alpha)$$

$$\vec{v}' = \underbrace{(\hat{n}^T \vec{v}) \hat{n}}_{\text{Components along } \hat{n} \text{ are preserved}} + \underbrace{(\vec{v} - (\hat{n}^T \vec{v}) \hat{n})}_{\text{x-component perpendicular to } \hat{n}} \cos \alpha + \underbrace{(\hat{n} \times \vec{v})}_{\text{y-component perpendicular to } \hat{n} \text{ and } \vec{v}} \sin \alpha$$

Components along \hat{n} are preserved

x-component perpendicular to \hat{n}

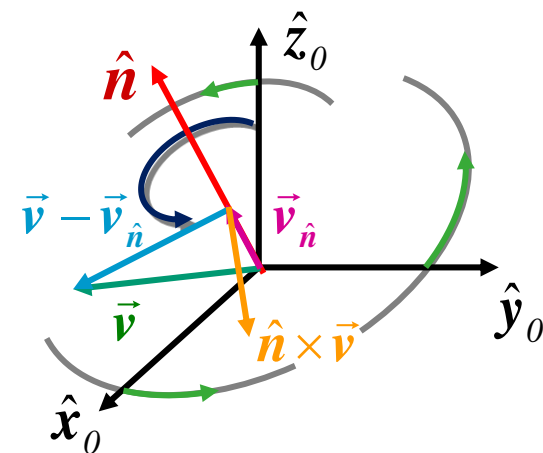
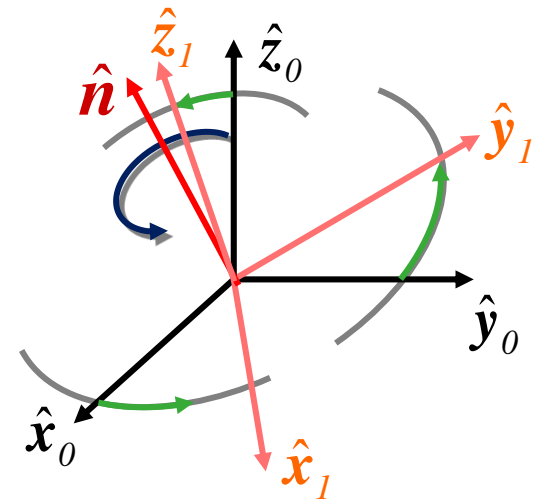
y-component perpendicular to \hat{n} and \vec{v}

- Matrix notation

$$\mathbf{R}(\hat{n}, \alpha) = \mathbf{P}_{\hat{n}} + (1 - \mathbf{P}_{\hat{n}}) \cos \alpha + \underbrace{\hat{n}^*}_{\text{cross product matrix}} \sin \alpha$$

using $\mathbf{P}_{\hat{n}} = \hat{n} \hat{n}^T$

cross product matrix





QUATERNIONS

Derivation of Euler Parameters



$$\vec{v}' = (\vec{v} \cdot \hat{n})\hat{n} + (\vec{v} - (\vec{v} \cdot \hat{n})\hat{n})\cos\alpha + (\hat{n} \times \vec{v})\sin\alpha$$

$$\vec{v}' = \vec{v} \cos\alpha + (\vec{v} \cdot \hat{n})\hat{n}(1 - \cos\alpha) + (\hat{n} \times \vec{v})\sin\alpha$$

addition theorems

$$\vec{v}' = \vec{v} \left(\cos^2 \frac{\alpha}{2} - \sin^2 \frac{\alpha}{2} \right) + 2(\vec{v} \cdot \hat{n})\hat{n} \sin^2 \frac{\alpha}{2} + 2(\hat{n} \times \vec{v}) \sin \frac{\alpha}{2} \cos \frac{\alpha}{2}$$

$$\vec{v}' = \left(e_0^2 - \|\vec{e}\|^2 \right) \vec{v} + 2(\vec{v} \cdot \vec{e})\vec{e} + 2e_0(\vec{e} \times \vec{v})$$

$$\begin{aligned} \sin 2x &= 2 \sin x \cos x \\ \cos 2x &= 1 - 2 \sin^2 x \\ \cos 2x &= \cos^2 x - \sin^2 x \end{aligned}$$

Eulerparameter

$$\begin{aligned} e_0 &= \cos \frac{\alpha}{2} \\ \vec{e} &= \hat{n} \sin \frac{\alpha}{2} = \begin{pmatrix} e_1 \\ e_2 \\ e_3 \end{pmatrix} \\ 1 &= \sum_{j=0}^3 e_j^2 \end{aligned}$$



Quaternion Definition

- comparison with complex numbers suggests definition of quaternions:

$$z = \cos \alpha + i \sin \alpha \quad \Leftrightarrow \quad q = e_0 + i e_1 + j e_2 + k e_3$$

- with complex roots i, j and k whose direct products define the rule of multiplying two quaternions
- when reducing to 2D rotations, the complex numbers should result. This implies

$$i^2 = j^2 = k^2 = ijk = -1$$

- This results in the following product table:
($ij = ji$ would result in a commutative product, but rotations in 3D don't commute)

*	1	i	j	k
1	1	i	j	k
i	i	-1	k	$-j$
j	j	$-k$	-1	i
k	k	j	$-i$	-1

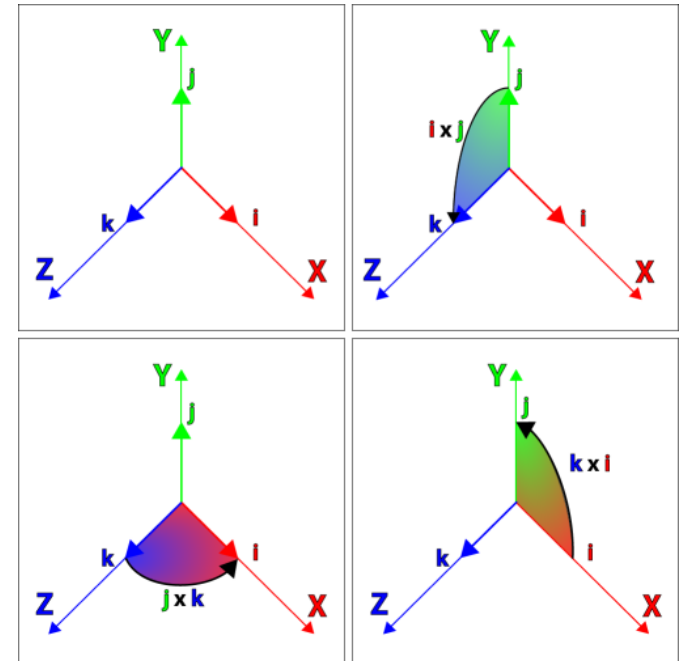
$k = ij$

Quaternion Definition

- Note the similarity between i, j, k and cross products of the orthogonal unit vectors $\hat{x}, \hat{y}, \hat{z}$:

*	1	i	j	k
1	1	i	j	k
i	i	-1	k	$-j$
j	j	$-k$	-1	i
k	k	j	$-i$	-1

\times	\hat{x}	\hat{y}	\hat{z}
\hat{x}	$\mathbf{0}$	\hat{z}	$-\hat{y}$
\hat{y}	$-\hat{z}$	$\mathbf{0}$	\hat{x}
\hat{z}	\hat{y}	$-\hat{x}$	$\mathbf{0}$



- detailed explanation of quaternions can be found at:
<http://3dgep.com/?p=1815>



More on Quaternions

- conjugation: $q^* = e_0 - e_1i - e_2j - e_3k$
- norm: $\|q\|^2 = qq^* = e_0^2 + e_1^2 + e_2^2 + e_3^2$
- inverse: $q^{-1} = \frac{1}{q} = \frac{q^*}{qq^*}$ for unit quaternions: $\hat{q}^{-1} = \hat{q}^*$
- scalar+vector-interpretation $q = (e_0, \vec{e}) = (s, \vec{v}) = (s, x, y, z)$
- multiplication $q_1q_2 = (s_1s_2 - \vec{v}_1 \cdot \vec{v}_2, s_1\vec{v}_2 + s_2\vec{v}_1 + \vec{v}_1 \times \vec{v}_2)$
- unit quaternions $\hat{q} = (\cos \frac{\alpha}{2}, \hat{n} \sin \frac{\alpha}{2})$ can be interpreted as rotation by α around \hat{n} . To rotate a 3d-vector \vec{p} construct quaternion $p = (0, \vec{p})$ and compute
$$p' = \hat{q}p\hat{q}^*$$
- efficient concatenation of rotations: $\hat{q}_{12} = \hat{q}_1\hat{q}_2$
- When interpolating rotations with quaternions one has to ensure that result is a proper rotation. Then one can normalize the result quaternion or use SLERP.

Example

- concatenation of rotation by α around x followed by rotation by β around y

- $q_x = \begin{pmatrix} \cos \frac{\alpha}{2} & \sin \frac{\alpha}{2} & 0 & 0 \end{pmatrix}$

- $q_y = \begin{pmatrix} \cos \frac{\beta}{2} & 0 & \sin \frac{\beta}{2} & 0 \end{pmatrix}$

- quat. product: $q_1 q_2 = (s_1 s_2 - \overrightarrow{\mathbf{v}}_1 \cdot \overrightarrow{\mathbf{v}}_2, s_1 \overrightarrow{\mathbf{v}}_2 + s_2 \overrightarrow{\mathbf{v}}_1 + \overrightarrow{\mathbf{v}}_1 \times \overrightarrow{\mathbf{v}}_2)$

$$q_y q_x = \begin{pmatrix} \cos \frac{\alpha}{2} \cos \frac{\beta}{2} & \sin \frac{\alpha}{2} \cos \frac{\beta}{2} & \cos \frac{\alpha}{2} \sin \frac{\beta}{2} & -\sin \frac{\alpha}{2} \sin \frac{\beta}{2} \end{pmatrix}$$

- this corresponds to rotation around new axis $\hat{\mathbf{n}}$ and new angle γ with

$$\hat{\mathbf{n}} = \begin{pmatrix} \sin \frac{\alpha}{2} \cos \frac{\beta}{2} & \cos \frac{\alpha}{2} \sin \frac{\beta}{2} & -\sin \frac{\alpha}{2} \sin \frac{\beta}{2} \end{pmatrix},$$



Example

- ◆ $q_y q_x = \left(\cos \frac{\alpha}{2} \cos \frac{\beta}{2} \quad \sin \frac{\alpha}{2} \cos \frac{\beta}{2} \quad \cos \frac{\alpha}{2} \sin \frac{\beta}{2} \quad - \sin \frac{\alpha}{2} \sin \frac{\beta}{2} \right)$

- ◆ this corresponds to rotation around new axis $\hat{\mathbf{n}}$ and new angle γ with

$$\vec{\mathbf{n}} = \left(\sin \frac{\alpha}{2} \cos \frac{\beta}{2} \quad \cos \frac{\alpha}{2} \sin \frac{\beta}{2} \quad - \sin \frac{\alpha}{2} \sin \frac{\beta}{2} \right),$$

$$\begin{aligned} \|\vec{\mathbf{n}}\|^2 &= \sin^2 \frac{\alpha}{2} \cos^2 \frac{\beta}{2} + \cos^2 \frac{\alpha}{2} \sin^2 \frac{\beta}{2} + \sin^2 \frac{\alpha}{2} \sin^2 \frac{\beta}{2} = \sin^2 \frac{\alpha}{2} \cos^2 \frac{\beta}{2} + \sin^2 \frac{\beta}{2}, \\ &= 1 - \cos^2 \frac{\beta}{2} + \sin^2 \frac{\alpha}{2} \cos^2 \frac{\beta}{2} = 1 - \cos^2 \frac{\beta}{2} \left(1 - \sin^2 \frac{\alpha}{2} \right) = 1 - \cos^2 \frac{\beta}{2} \cos^2 \frac{\alpha}{2} \end{aligned}$$

$$\hat{\mathbf{n}} = \frac{1}{\sqrt{1 - \cos^2 \frac{\beta}{2} \cos^2 \frac{\alpha}{2}}} \left(\sin \frac{\alpha}{2} \cos \frac{\beta}{2} \quad \cos \frac{\alpha}{2} \sin \frac{\beta}{2} \quad - \sin \frac{\alpha}{2} \sin \frac{\beta}{2} \right),$$

- ◆ and angle

$$\gamma = \arctan2 \left(\sqrt{1 - \cos^2 \frac{\beta}{2} \cos^2 \frac{\alpha}{2}}, \cos \frac{\alpha}{2} \cos \frac{\beta}{2} \right)$$



- conversion to rotation matrix can be derived by transforming the base vectors \hat{x} , \hat{y} , \hat{z} with the quaternion and writing result in columns of rotation matrix:

$$\mathbf{R} \left(q = \begin{pmatrix} s \\ x \\ y \\ z \end{pmatrix} \right) = \begin{pmatrix} s^2 + x^2 - y^2 - z^2 & 2(xy - sz) & 2(xz + sy) \\ 2(xy + sz) & s^2 - x^2 + y^2 - z^2 & 2(yz - sx) \\ 2(xz - sy) & 2(yz + sx) & s^2 - x^2 - y^2 + z^2 \end{pmatrix}$$

- conversion back to quaternion from diagonal elements of \mathbf{R} and normalization constraint:

$$\begin{pmatrix} 1 & 1 & -1 & -1 \\ 1 & -1 & 1 & -1 \\ 1 & -1 & -1 & 1 \\ 1 & 1 & 1 & 1 \end{pmatrix} \begin{pmatrix} s^2 \\ x^2 \\ y^2 \\ z^2 \end{pmatrix} = \begin{pmatrix} R_{xx} \\ R_{yy} \\ R_{zz} \\ 1 \end{pmatrix} \Rightarrow \begin{pmatrix} s^2 \\ x^2 \\ y^2 \\ z^2 \end{pmatrix} = \frac{1}{4} \begin{pmatrix} 1 & 1 & 1 & 1 \\ 1 & -1 & -1 & 1 \\ -1 & 1 & -1 & 1 \\ -1 & -1 & 1 & 1 \end{pmatrix} \begin{pmatrix} R_{xx} \\ R_{yy} \\ R_{zz} \\ 1 \end{pmatrix}$$

- The signs of the components can be derived from ([see](#))
 $s = 1; x = \text{sgn}(R_{zy} - R_{yz}); y = \text{sgn}(R_{xz} - R_{zx}); z = \text{sgn}(R_{yx} - R_{xy});$

- Example of derivation of x-column of rotation matrix:

$$\hat{q} = (s, \begin{pmatrix} x \\ y \\ z \end{pmatrix}) \quad q_1 q_2 = (s_1 s_2 - \vec{v}_1 \cdot \vec{v}_2, s_1 \vec{v}_2 + s_2 \vec{v}_1 + \vec{v}_1 \times \vec{v}_2) \quad \hat{q}^* = (s, \begin{pmatrix} -x \\ -y \\ -z \end{pmatrix})$$

$$\begin{aligned} \hat{q} \begin{pmatrix} 0 \\ \begin{pmatrix} 1 \\ 0 \\ 0 \end{pmatrix} \end{pmatrix} \hat{q}^* &= \begin{pmatrix} -x, \begin{pmatrix} s \\ z \\ -y \end{pmatrix} \end{pmatrix} \hat{q}^* = \begin{pmatrix} \overbrace{-xs - (-xs - zy + yz)}^0, \\ -x \begin{pmatrix} -x \\ -y \\ -z \end{pmatrix} + s \begin{pmatrix} s \\ z \\ -y \end{pmatrix} + \begin{pmatrix} s \\ z \\ -y \end{pmatrix} \times \begin{pmatrix} -x \\ -y \\ -z \end{pmatrix} \end{pmatrix} \\ &= \begin{pmatrix} 0, \begin{pmatrix} s^2 - x^2 \\ xy + sz \\ xz - sy \end{pmatrix} + \begin{pmatrix} y^2 - z^2 \\ xy + sz \\ xz - sy \end{pmatrix} \end{pmatrix} \\ &= \begin{pmatrix} 0, \begin{pmatrix} s^2 - x^2 + y^2 - z^2 \\ 2(xy + sz) \\ 2(xz - sy) \end{pmatrix} \end{pmatrix} \end{aligned}$$

Double Cover of Rotations

- The axis-angle representation of rotations with $\alpha \in]-\pi, \pi]$ is not unique, as

$$\mathbf{R}(\hat{\mathbf{n}}, \alpha) = \mathbf{R}(-\hat{\mathbf{n}}, -\alpha)$$

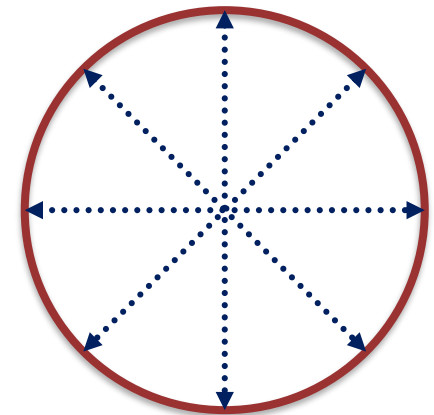
- Each rotation has two representations. We call this a double cover of the group of rotations
- The quaternions are also a double cover as

$$qpq^* = (-q)p(-q^*)$$

with

$$\begin{aligned}
 -q &= \left(-\cos \frac{\alpha}{2} \quad -\sin \frac{\alpha}{2} \hat{\mathbf{n}} \right) = \\
 &\begin{pmatrix} \cos \left(\pi - \frac{\alpha}{2} \right) & \sin \left(\pi - \frac{\alpha}{2} \right) (-\hat{\mathbf{n}}) \\ \cos \frac{2\pi - \alpha}{2} & \sin \frac{2\pi - \alpha}{2} (-\hat{\mathbf{n}}) \end{pmatrix} =
 \end{aligned}$$

- On the 3-unit sphere in 4D space the unit quaternions that are related by point reflection at origin represent same rotation





2D

Pktrep. Rotrep. Transf.

■ 2x2 Matrix

$$\vec{p} = \begin{pmatrix} x \\ y \end{pmatrix} \begin{pmatrix} \cos \alpha & -\sin \alpha \\ \sin \alpha & \cos \alpha \end{pmatrix} \mathbf{T}_{\text{rot}} \vec{p}$$

■ komplexe Zahlen

$$z = x + iy \quad e^{i\alpha} = \cos \alpha + i \sin \alpha \quad ze^{i\alpha} = e^{i\alpha} z$$

3D

Pktrep. Rotrep. Transf.

■ 3x3 Matrix

$$\vec{p} = \begin{pmatrix} x \\ y \\ z \end{pmatrix} \begin{pmatrix} 1 & 0 & 0 \\ 0 & \cos \alpha & -\sin \alpha \\ 0 & \sin \alpha & \cos \alpha \end{pmatrix} \mathbf{T}_{\text{rot}} \vec{p}$$

■ Quaternionen

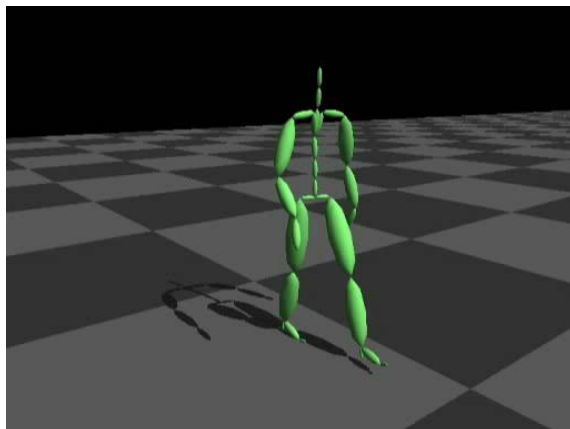
$$p = (0, \vec{p}) = xi + yj + zk \quad q = \left(\cos \frac{\alpha}{2}, \hat{n} \sin \frac{\alpha}{2} \right) = \cos \frac{\alpha}{2} + \sin \frac{\alpha}{2} (n_x i + n_y j + n_z k) \quad qpq^{-1} = qpq^*$$



ARTICULATED OBJECTS



© <http://the-4thworld.com/essentials.html>



Fabricating Articulated Characters from Skinned Meshes

SIGGRAPH 2012

Moritz Bächer, Harvard University

Bernd Bickel, TU Berlin

Doug L. James, Cornell University

Hanspeter Pfister, Harvard University

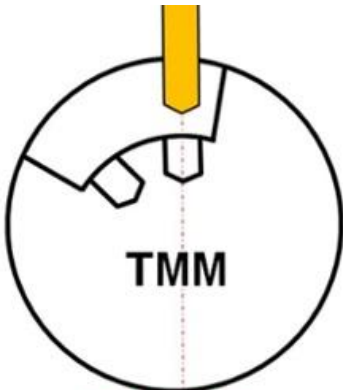
Fabricating Articulated Characters
using Skinned Meshes, Siggraph 2012

Motivation – CNC-Milling Machines

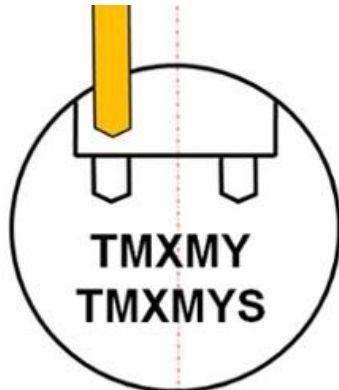


X&C3-Axes only

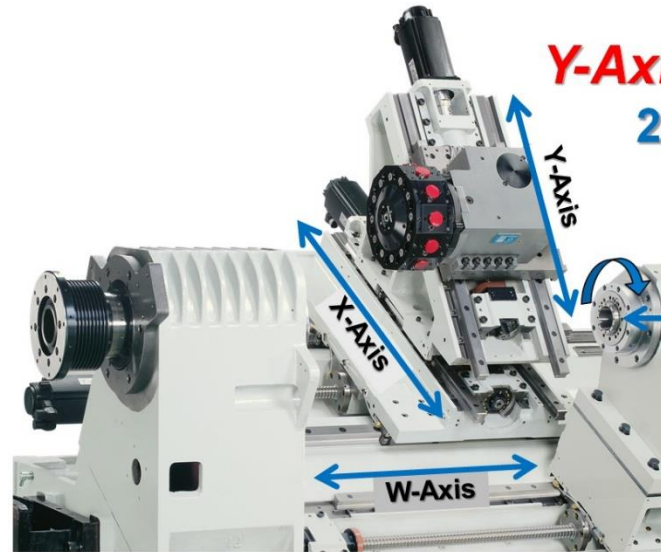
Y-Axis needed



C-Axis Drilling
(always points to center)



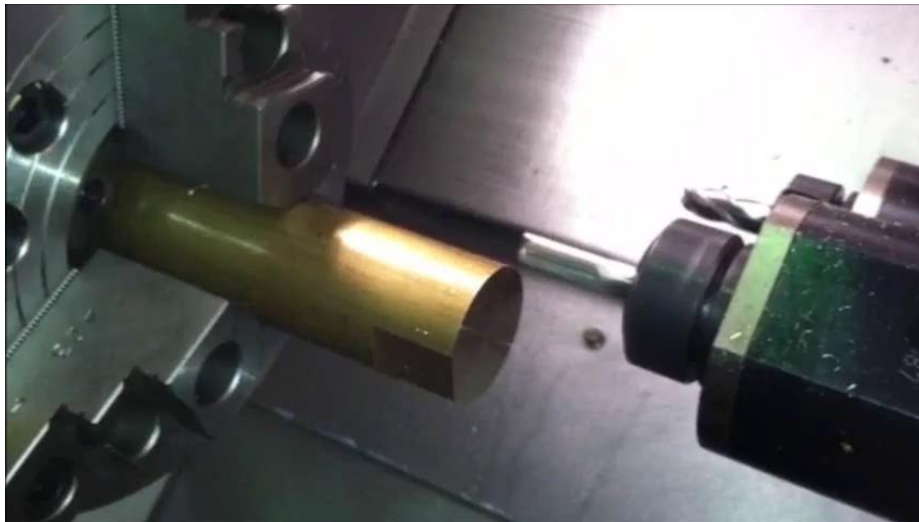
Y-Axis Drilling
(allowed to move laterally)



Y-Axis Configuration 2-axis Wedge Design

- X-Axis
 - Used to compensate for clearance of the moving Y-axis
- Y-Axis
 - Programmed as perpendicular plane to the X-axis.

C3-Axis
(sub-spindle)



X&C3-Axes only flats



X&C3-Axes only circle

<http://blog.hurco.com/blog/bid/281989/An-Introduction-to-Mill-Turn-Technology>

Motivation – Skeletal Animation

biped body tracking

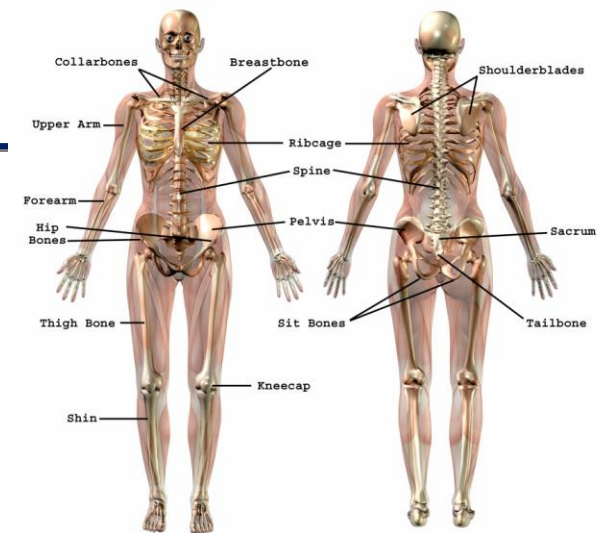
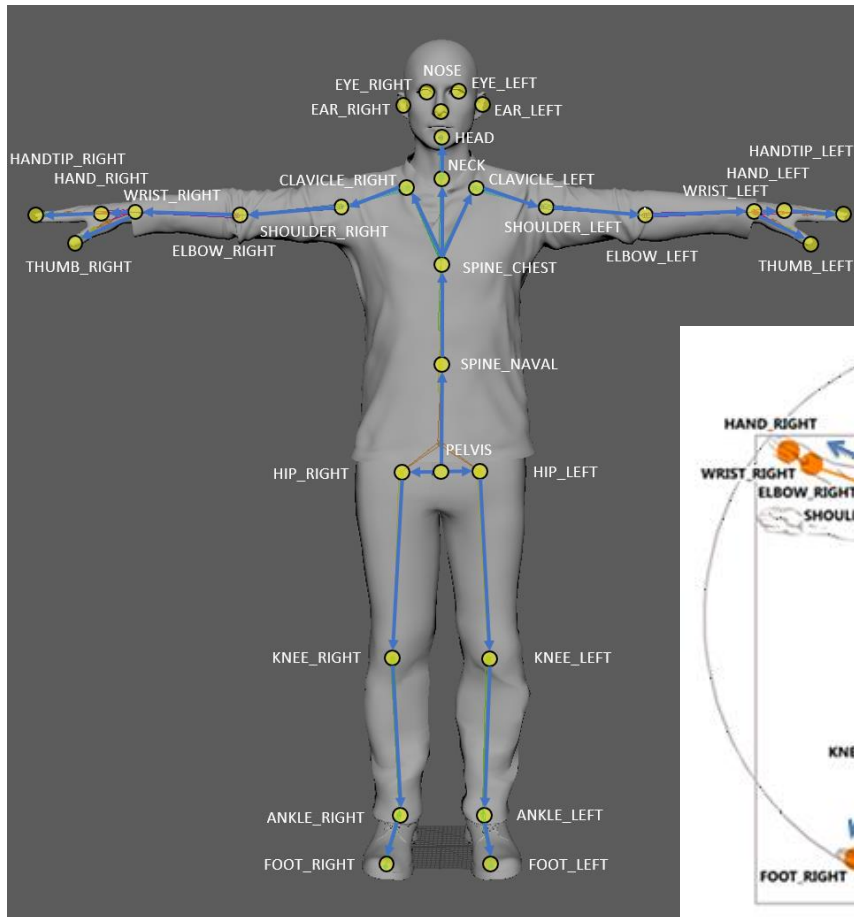
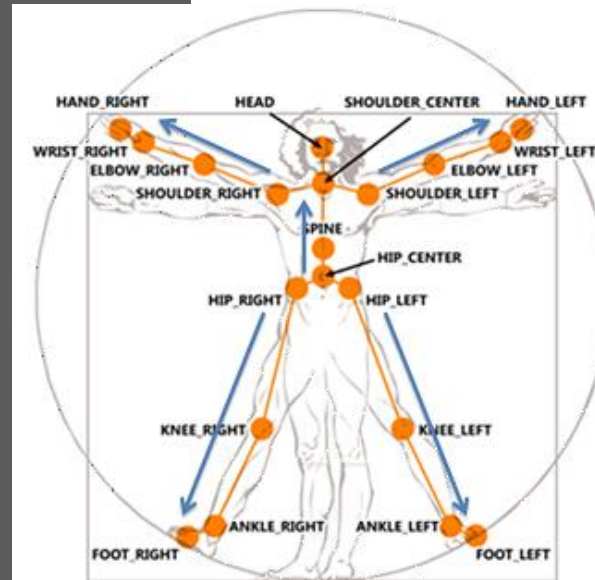


illustration of human skeleton

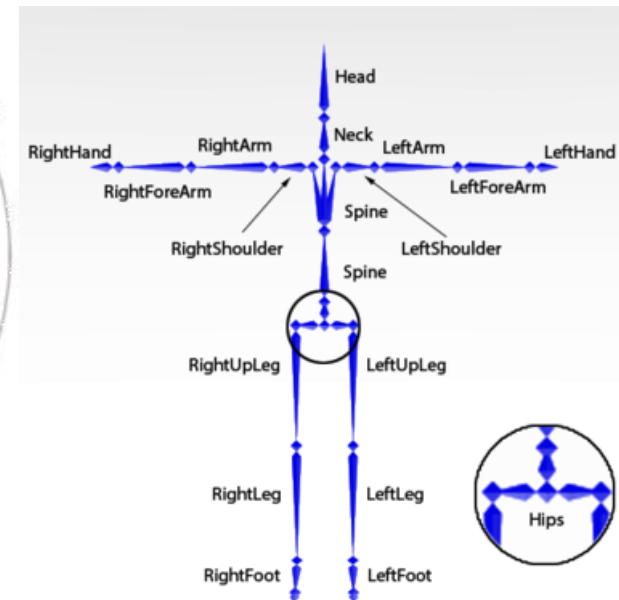
© <http://insectanatomy.com/tag/bones-names>



kinect azure skeleton



kinect 1.0 skeleton

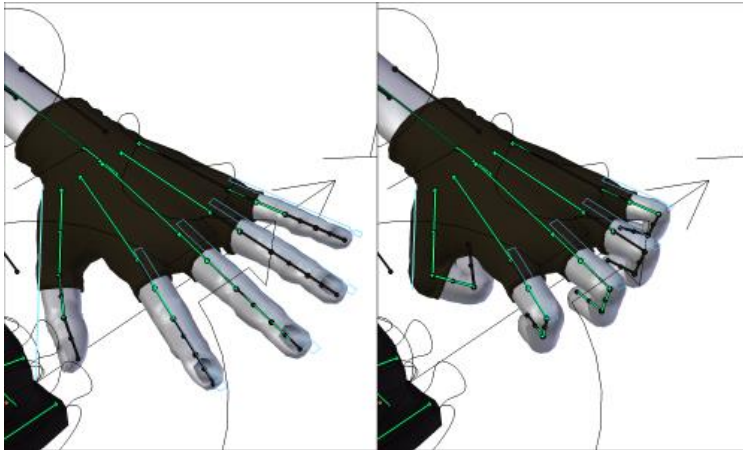


BVH skeleton

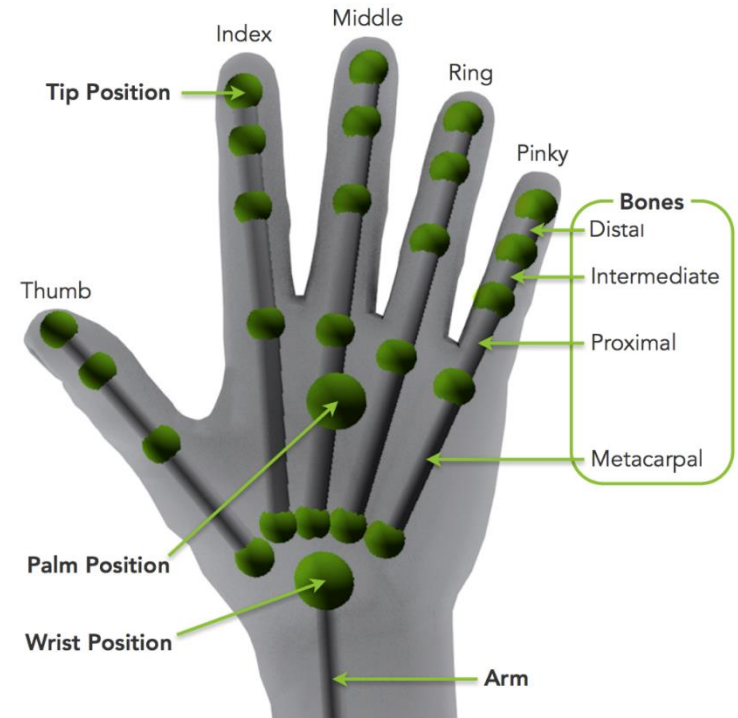
(mocap file format: Biovision

hierarchical data) 29

hand tracking



© wikipedia

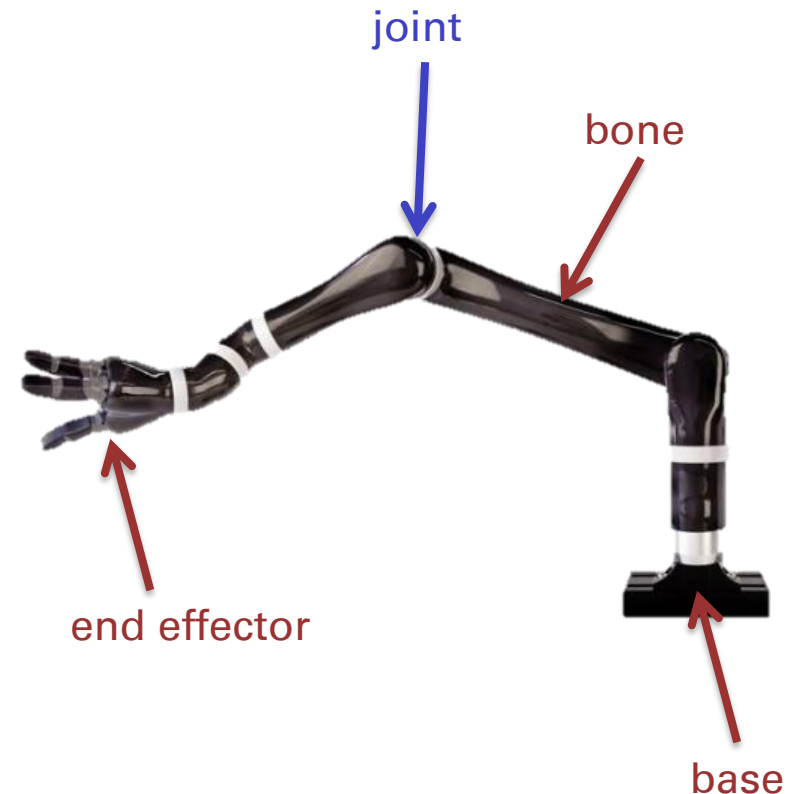


leap motion hand skeleton

Other applications: facial animations

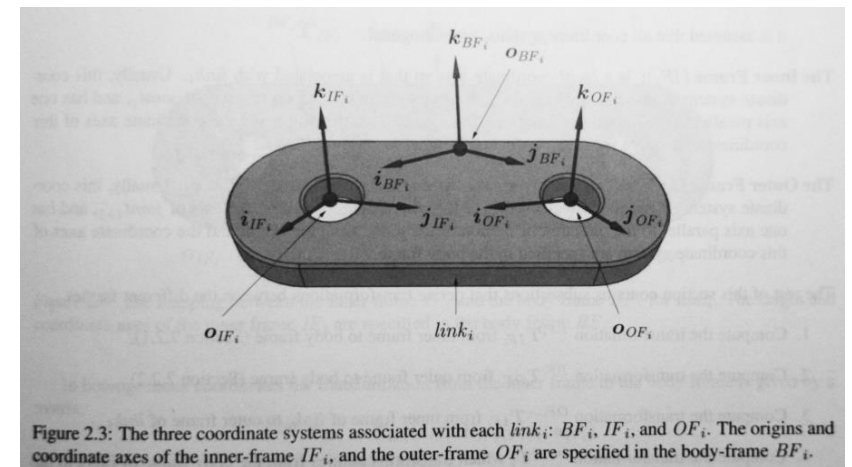
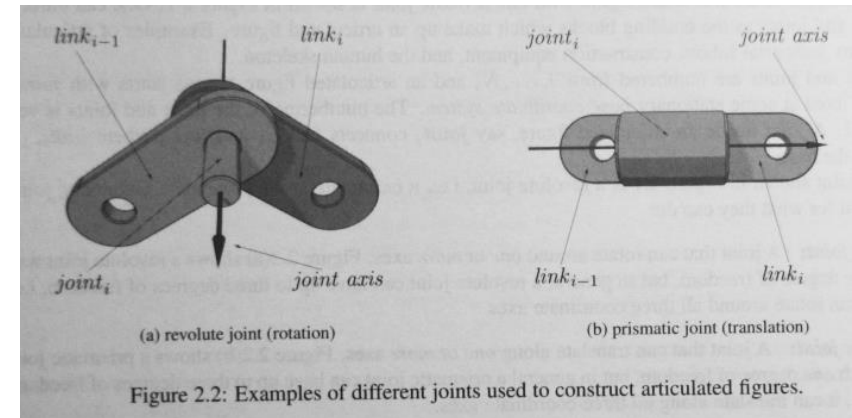
Kinematic Chain – Definition

- ◆ **bone/limb/link** corresponds to a stiff part and a bone coordinate system
- ◆ the arm is fixed at the first bone, which is called **base**
- ◆ the last bone is also called **end effector** and used for example for grabbing
- ◆ **joints** connect two bones and often have an own coordinate system aligned with their rotation axis
- ◆ bones and joints form a **kinematic chain**



Robot arms with Bones and Joints

- ◆ In robotics and milling the most basic joint types are **revolute** and **prismatic joints** with one axis each
- ◆ per bone three coordinate systems are defined:
 - ◆ **input joint** (subscript I) is reference coordinate system of bone
 - ◆ **bone** (subscript B) is used to place bone geometry
 - ◆ **output joint** (subscript O) is used to connect next bone
- ◆ joint coordinate systems are aligned with joint axis



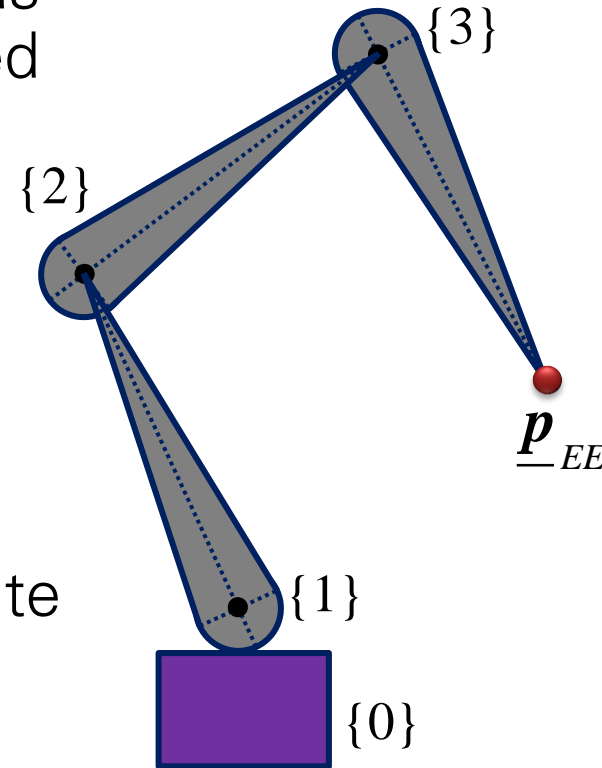
Kinematic Chain – Coordinate Systems



- input joint coordinate systems are used as reference for base / bone and enumerated from 0 (base/world) to N (end effector)
- Transformations are composed along kinematic chain

$${}^0\mathbf{T}_N = {}^0\mathbf{T}_1 \cdot {}^1\mathbf{T}_2 \cdot \dots \cdot {}^{N-1}\mathbf{T}_N$$

- model transform view*: place bones from base to end effector
- system transform view*: convert coordinate system from end effector to base
- This can be further refined into

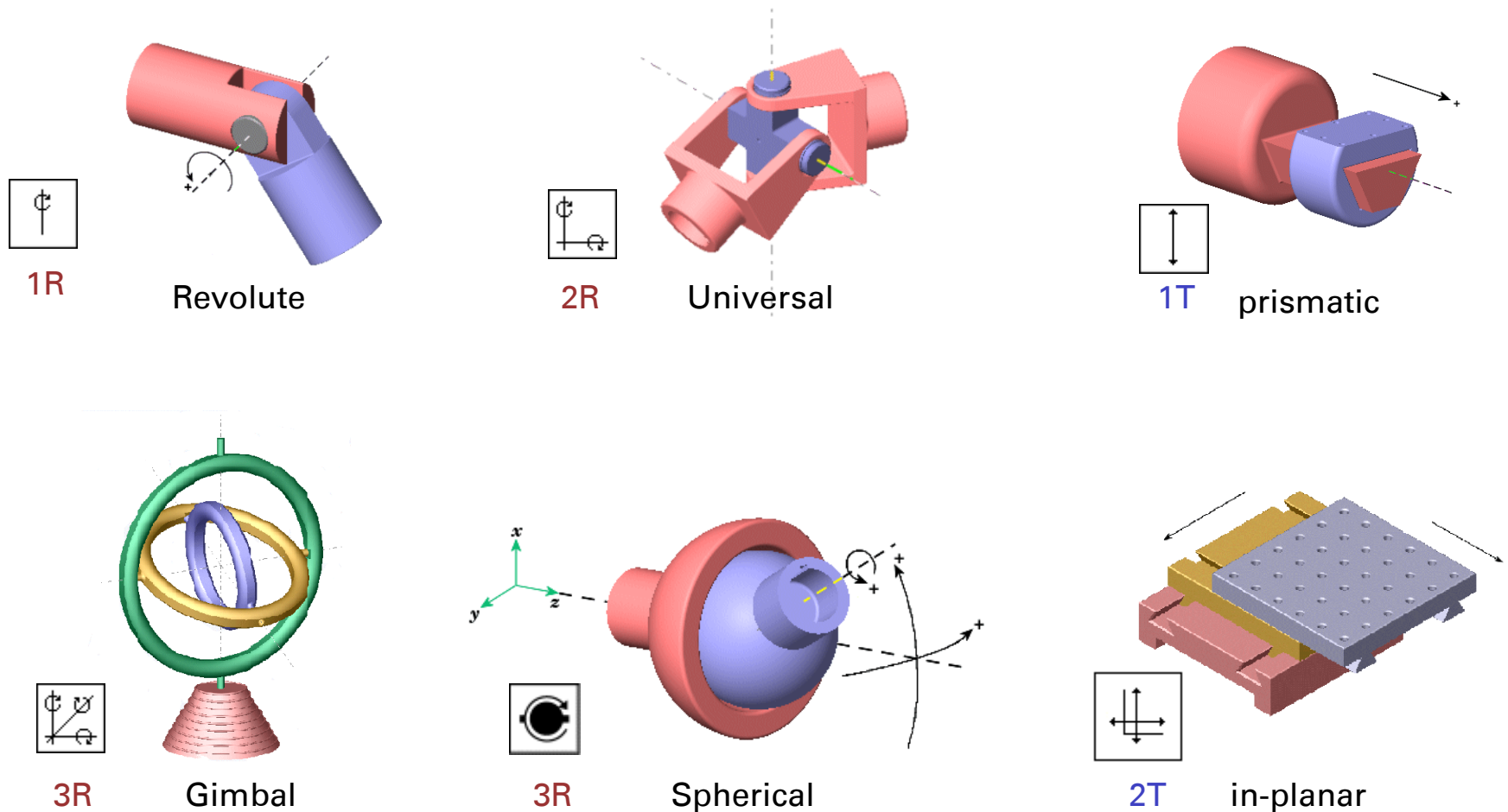


$$\mathbf{T}_{\text{chain}} = \underbrace{{}^{\text{world}}\mathbf{T}_{OF_0}}_{{}^0\mathbf{T}_1} \cdot \underbrace{{}^{OF_0}\mathbf{T}_{IF_1}}_{{}^1\mathbf{T}_2} \cdot \underbrace{{}^{IF_1}\mathbf{T}_{BF_1} \cdot {}^{BF_1}\mathbf{T}_{OF_1}}_{{}^2\mathbf{T}_3} \cdot \underbrace{{}^{OF_1}\mathbf{T}_{IF_2} \cdot {}^{IF_2}\mathbf{T}_{BF_2} \cdot {}^{BF_2}\mathbf{T}_{OF_2}}_{{}^3\mathbf{T}_4} \cdot \dots \cdot {}^{IF_{\text{end}}}\mathbf{T}_{BF_{\text{end}}}$$

← **local joint transformations** →

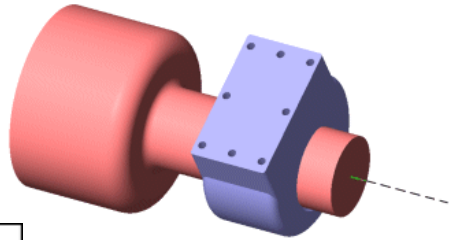
← **dependent on joint parameters** →

Basic Joint Types

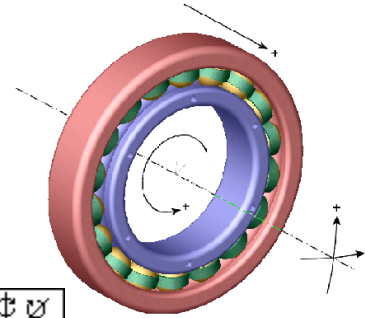


<http://www.mathworks.de/de/help/physmod/sm/assembled-joints.html>

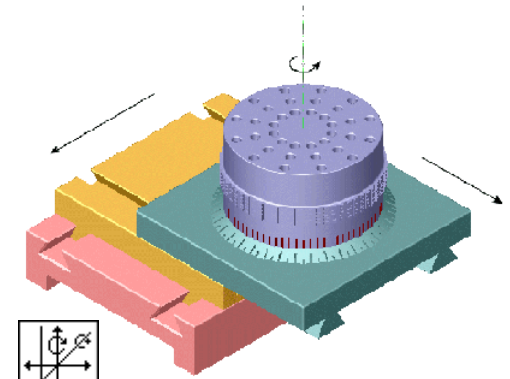
Special Joint Types



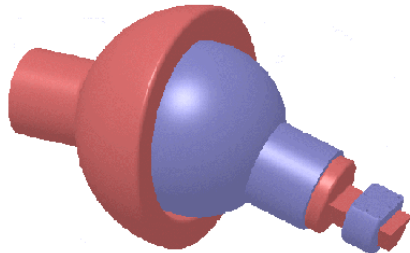
1R1T Cylindrical



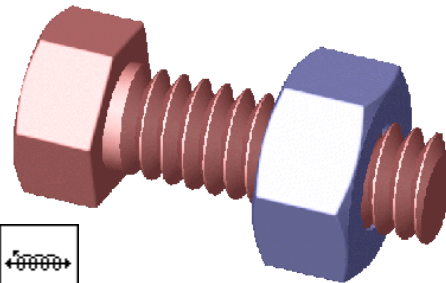
3R1T Bearing



1R2T planar



3R1T Telescoping



Screw

Six-DoF



3R3T

Bushing



3R3T

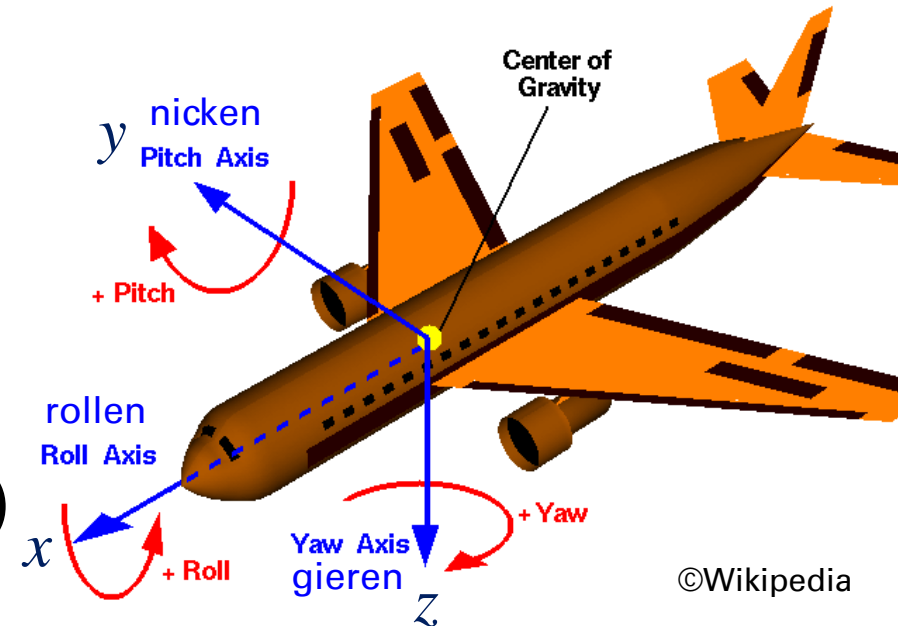
<http://www.mathworks.de/de/help/physmod/sm/assembled-joints.html>



Roll-Pitch-Yaw

- An arbitrary rotation is defined by 3 free parameters
- They can be defined by 3 rotation angles which are called Euler angles
- Coming from aeronautics, the terms roll (x), pitch (y) and yaw (z) are commonly used

$$\mathbf{R}_{\text{roll-pitch-yaw}} = \mathbf{R}_Z(\phi_{\text{yaw}})\mathbf{R}_Y(\phi_{\text{pitch}})\mathbf{R}_X(\phi_{\text{roll}})$$

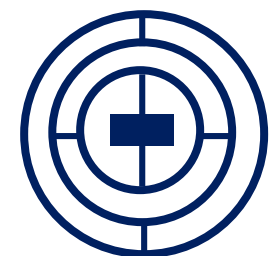
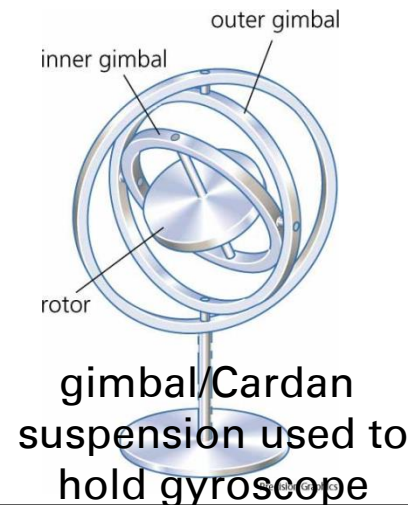


©Wikipedia

Navigation using gyroscopes

- Commonly used: 313-Convention
- The first and third axis can become parallel, thus reducing one degree of freedom. This is called "gimbal lock".

$$\mathbf{R}_{313}(\alpha, \beta, \gamma) = \mathbf{R}_Z(\alpha)\mathbf{R}_X(\beta)\mathbf{R}_Z(\gamma)$$



gimbal lock
only 2R left

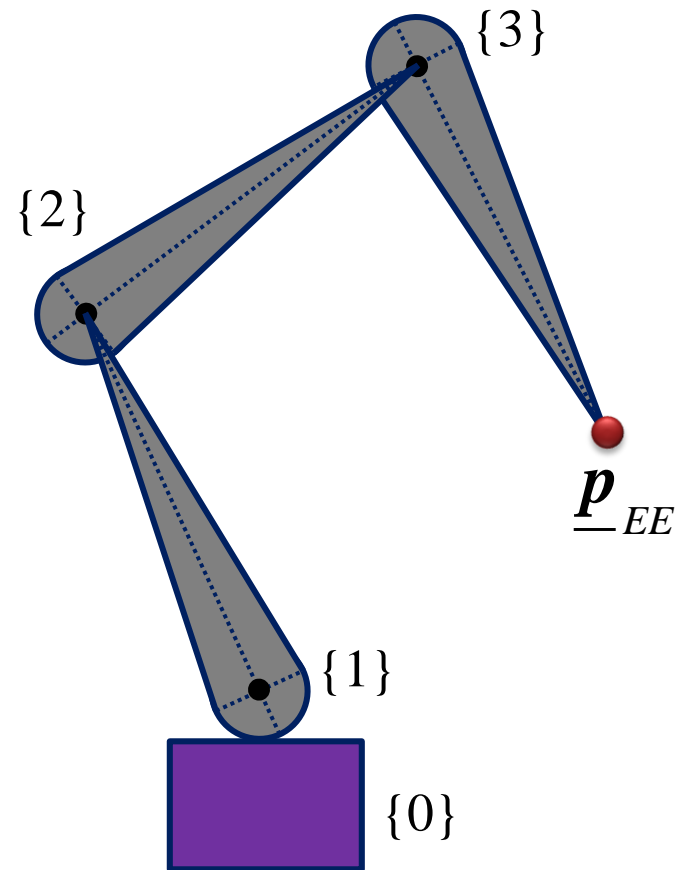
Forward Kinematics

- Given a kinematic chain (robot arm or path in skeleton) with relative transformations ${}^{(i-1)}T_i(q_{ik})$ depending on **parameters** q_{ik} location and orientation of the end effector in world coordinates are a function of the q_{ik} also:

$$\underline{p}_{EE}^0 = {}^0T_N \underline{p}_{EE}^N = \underline{f}(q_{ik})$$

$$\omega_{EE}^0 = R_{313}^{-1} \left({}^0T_N \Big|_{\underline{xyz}} \right) = \underline{F}(q_{ik})$$

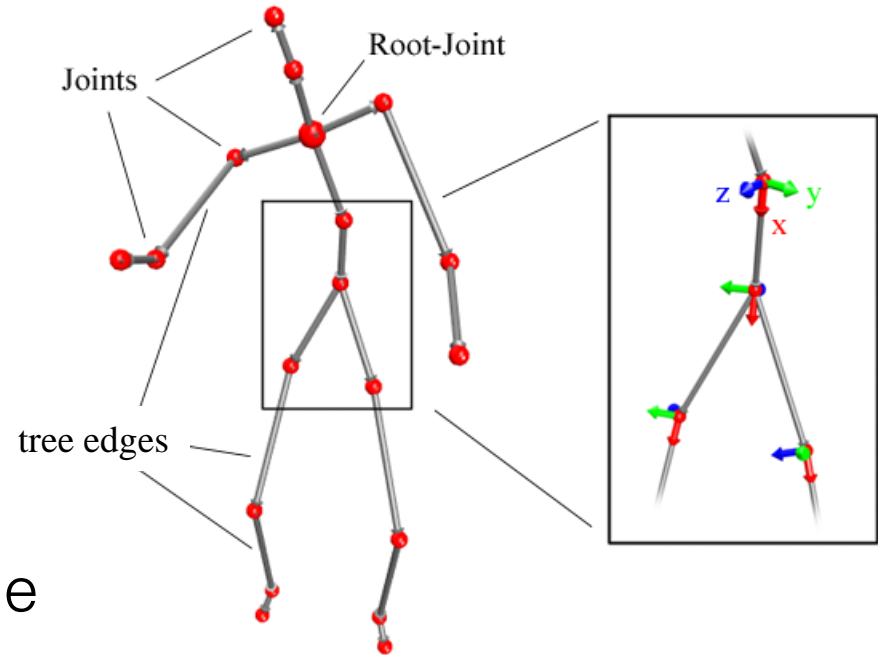
Orientation for example given as Euler angles and computed from 3x3-rotation matrix



$${}^0T_N = {}^0T_1 \cdot {}^1T_2 \cdot \dots \cdot {}^{N-1}T_N$$

Kinematic Tree / Skeleton

- ◆ a skeleton is a **kinematic tree** structure with joints as nodes and bones along edges.
- ◆ it has a single root joint and **several end effectors**
- ◆ at each joint i a joint coordinate frame F_i is defined
- ◆ **Local joint transformations** $p^{(i)}\mathbf{T}_i$ map from parent frame $F_{p(i)}$ to F_i with a rigid body transformation
- ◆ together all local joint transforms define the **pose of the skeleton**



© Stefan Bröcker



- In the Denavit-Hartenberg notation for each link there is one adjustable parameter q_{ik} corresponding to d_i or φ_i depending on the joint type (prismatic or revolution)

$${}^{i-1}\mathbf{T}_i(d_i \vee \varphi_i) = \begin{pmatrix} \cos \varphi_i & -\sin \varphi_i & 0 & a_{i-1} \\ \sin \varphi_i \cos \alpha_{i-1} & \cos \varphi_i \cos \alpha_{i-1} & -\sin \alpha_{i-1} & -d_i \sin \alpha_{i-1} \\ \sin \varphi_i \sin \alpha_{i-1} & \cos \varphi_i \sin \alpha_{i-1} & \cos \alpha_{i-1} & d_i \cos \alpha_{i-1} \\ 0 & 0 & 0 & 1 \end{pmatrix}$$

- Using Euler angles one has 6 parameters

$${}^{i-1}\mathbf{T}_i(\alpha_i, \beta_i, \gamma_i, \vec{t}_i) = \mathbf{T}(\vec{t}_i) \mathbf{R}_Z(\gamma_i) \mathbf{R}_X(\beta_i) \mathbf{R}_Z(\alpha_i) = \begin{bmatrix} \cos(\gamma_i) \cos(\alpha_i) - \sin(\gamma_i) \cos(\beta_i) \sin(\alpha_i) & -\cos(\gamma_i) \sin(\alpha_i) - \sin(\gamma_i) \cos(\beta_i) \cos(\alpha_i) & \sin(\gamma_i) \sin(\beta_i) & t_x \\ \sin(\gamma_i) \cos(\alpha_i) + \cos(\gamma_i) \cos(\beta_i) \sin(\alpha_i) & -\sin(\gamma_i) \sin(\alpha_i) + \cos(\gamma_i) \cos(\beta_i) \cos(\alpha_i) & -\cos(\gamma_i) \sin(\beta_i) & t_y \\ \sin(\beta_i) \sin(\alpha_i) & \sin(\beta_i) \cos(\alpha_i) & \cos(\beta_i) & t_z \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

- Using quaternions one has 7 parameters plus one normalization constraint

$$s^2 + x^2 + y^2 + z^2 = 1$$

$${}^{i-1}\mathbf{T}_i(q_i = (s, x, y, z), \vec{t}_i) =$$

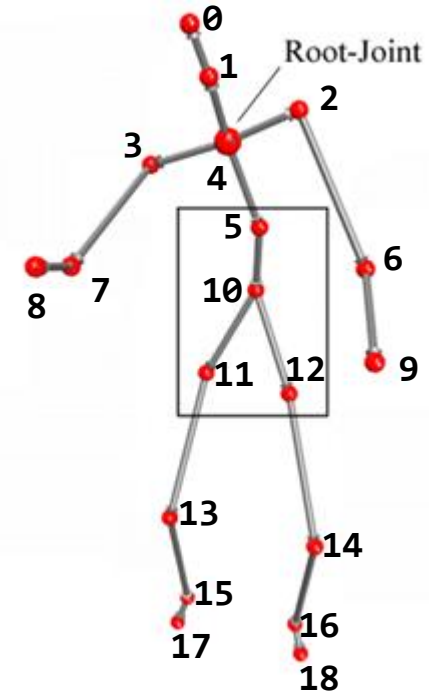
$$\begin{pmatrix} 1-2y^2-2z^2 & 2xy-2sz & 2xz+2ys & t_x \\ 2xy+2sz & 1-2x^2-2z^2 & 2yz-2sx & t_y \\ 2xz-2sy & 2yz+2sx & 1-2x^2-2y^2 & t_z \\ 0 & 0 & 0 & 1 \end{pmatrix}$$

Computing Joint to World Transforms



joint index	4	3	2	1	5	7	6	0	10	8	9	11	12	13	14	15	16	17	18
p(i)	-1	0	0	0	0	1	2	3	4	5	6	8	8	11	12	13	14	15	16

- the skeleton tree can be linearized in breadth or depth first traversal
- for rendering we need for each joint the **joint to world transformation** 0T_i
- these transformations can be stored linearly in **breadth or depth first order**
- Both orders guarantee that parent to world transformation is computed before joint to world transformation, allowing for **sequential computation**:



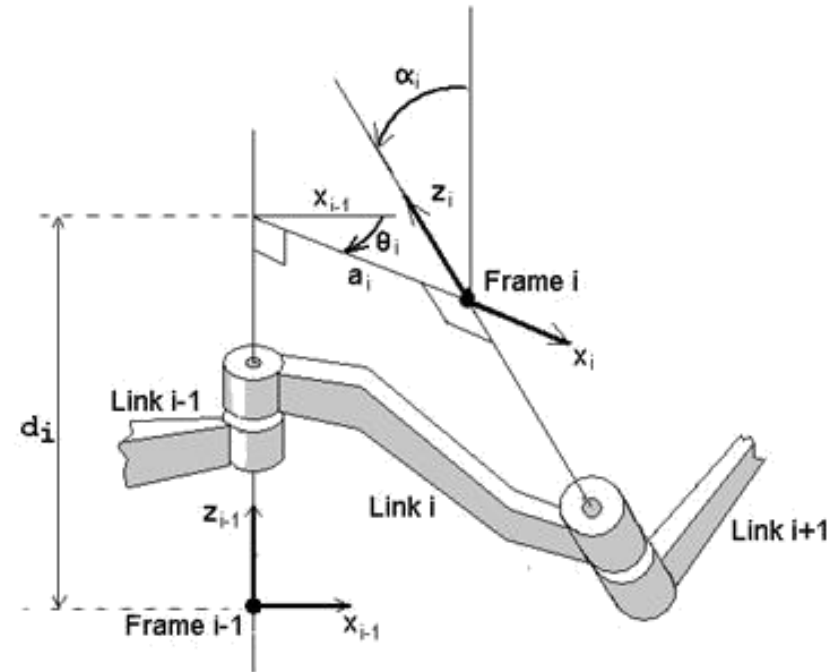
initialize 0T_1
 for i from 1 to n do

$${}^0T_i = {}^0T_{p(i)} p^{(i)} T_i(q_{ik})$$

DENAVIT-HARTENBERG NOTATION

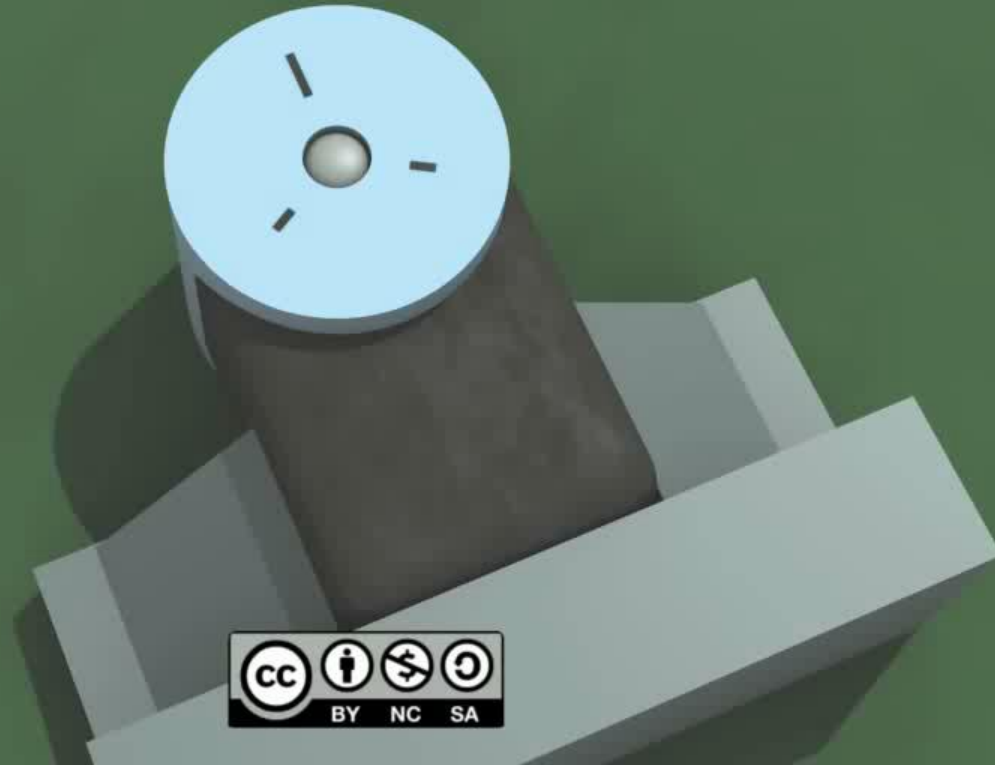
Denavit-Hartenberg notation

- ◆ **input:** joint axes $\underline{p}_i + \lambda \cdot \hat{z}_i$
 - ◆ **output:** joint input coordinate frames $\underline{o}_i, \hat{x}_i, \hat{y}_i, \hat{z}_i$ and four parameters d_i, θ_i, a_i and α_i per joint:
 - ◆ d_i ... is the Euclidean distance along axis \hat{z}_{i-1} to the point where the common perpendicular intersects axis \hat{z}_{i-1} . (parameter of prismatic variable)
 - ◆ θ_i ... joint angle / rotation angle around \hat{z}_{i-1} that rotates \hat{x}_{i-1} axis onto \hat{x}_i axis (parameter of revolute joint)
 - ◆ a_i ... link length / perp. distance between joint axes
 - ◆ α_i ... link twist / rotation angle between joint axes (around \hat{x}_i)
- $\rightarrow {}^{i-1}T_i = \text{Rot}_z(\theta_i) \cdot \text{Trans}_z(d_i) \cdot \text{Trans}_x(a_i) \cdot \text{Rot}_x(\alpha_i)$
- ◆ x-axis of base can be chosen freely



Denavit–Hartenberg Reference Frame Layout

Produced by Ethan Tira–Thompson



here $a_i, \alpha_i, d_i, \varphi_i$ are denoted as r, α, d, θ_i

<https://www.youtube.com/watch?v=rA9tm0gTln8>



- new $\hat{\mathbf{x}}_i$ axis is perpendicular to both $\hat{\mathbf{z}}$ axes:

$$\hat{\mathbf{x}}_i = \pm \text{normalize}(\hat{\mathbf{z}}_{i-1} \times \hat{\mathbf{z}}_i)$$

- sign of $\hat{\mathbf{x}}_i$ is determined from constraint that $a_i > 0$, where a_i is the projected distance from $\underline{\mathbf{p}}_i$ to $\underline{\mathbf{p}}_{i+1}$: $a_i = \langle \underline{\mathbf{p}}_{i+1} - \underline{\mathbf{p}}_i, \hat{\mathbf{x}}_i \rangle$

- we get from origin $\underline{\mathbf{o}}_{i-1}$ to $\underline{\mathbf{o}}_i$ along the path

$$\underline{\mathbf{o}}_i = \underline{\mathbf{o}}_{i-1} + d_i \hat{\mathbf{z}}_{i-1} + a_i \hat{\mathbf{x}}_i$$

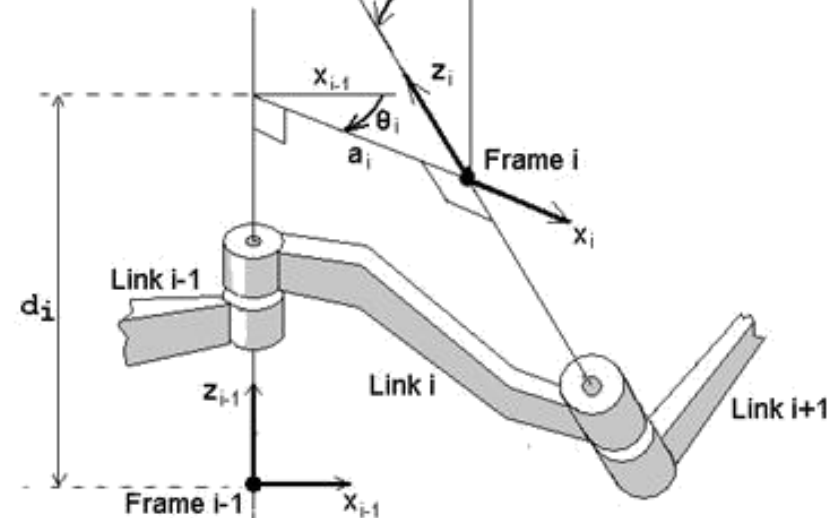
- $\underline{\mathbf{o}}_i$ is on axis i : $\underline{\mathbf{o}}_i = \underline{\mathbf{p}}_i + \lambda \cdot \hat{\mathbf{z}}_i = \underline{\mathbf{o}}_{i-1} + d_i \hat{\mathbf{z}}_{i-1} + a_i \hat{\mathbf{x}}_i$

- we can compute d_i and λ by forming triple products:

$$d_i = \langle \underline{\mathbf{p}}_i - \underline{\mathbf{o}}_{i-1}, \hat{\mathbf{z}}_i \times \hat{\mathbf{x}}_i \rangle / \langle \hat{\mathbf{z}}_{i-1}, \hat{\mathbf{z}}_i \times \hat{\mathbf{x}}_i \rangle$$

$$\lambda = \langle \underline{\mathbf{o}}_{i-1} - \underline{\mathbf{p}}_i, \hat{\mathbf{z}}_{i-1} \times \hat{\mathbf{x}}_i \rangle / \langle \hat{\mathbf{z}}_i, \hat{\mathbf{z}}_{i-1} \times \hat{\mathbf{x}}_i \rangle$$

- The frames are completed with $\hat{\mathbf{y}}_i = \hat{\mathbf{z}}_i \times \hat{\mathbf{x}}_i$





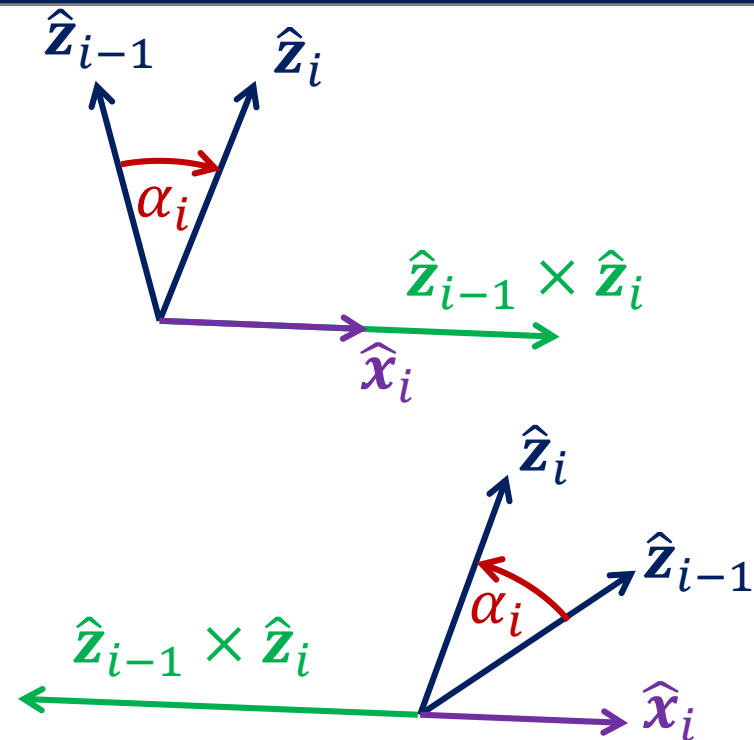
DH 360° Angle Computation

- Take care when computing angles via **arctan2** through $\sin \alpha_i = \|\hat{\mathbf{z}}_{i-1} \times \hat{\mathbf{z}}_i\|$ and $\cos \alpha_i = \langle \hat{\mathbf{z}}_{i-1}, \hat{\mathbf{z}}_i \rangle$
- As the sine is always positive, the range of α_i is $[0, \pi]$
- One needs to determine the sign of α_i from the sign of $\langle \hat{\mathbf{z}}_{i-1} \times \hat{\mathbf{z}}_i, \hat{\mathbf{x}}_i \rangle$, i.e.

$$\alpha_i = \text{sgn}(\langle \hat{\mathbf{z}}_{i-1} \times \hat{\mathbf{z}}_i, \hat{\mathbf{x}}_i \rangle) \cdot \arctan2(\|\hat{\mathbf{z}}_{i-1} \times \hat{\mathbf{z}}_i\|, \langle \hat{\mathbf{z}}_{i-1}, \hat{\mathbf{z}}_i \rangle)$$

- Similarly one gets

$$\theta_i = \text{sgn}(\langle \hat{\mathbf{x}}_{i-1} \times \hat{\mathbf{x}}_i, \hat{\mathbf{z}}_{i-1} \rangle) \cdot \arctan2(\|\hat{\mathbf{x}}_{i-1} \times \hat{\mathbf{x}}_i\|, \langle \hat{\mathbf{x}}_{i-1}, \hat{\mathbf{x}}_i \rangle)$$



- ◆ [Spong] ... Mark W. Spong, Seth Hutchinson, and M. Vidyasagar, Robot Dynamics and Control (2nd Edition), 2004, [Chapter 3 – Forward Kinematics: DH Convention](#)
- ◆ [Bächer] ... Moritz Bächer, Bernd Bickel, Doug L. James, and Hanspeter Pfister. 2012. Fabricating articulated characters from skinned meshes. *ACM Trans. Graph.* 31, 4, Article 47 (July 2012), 9 pages. DOI: <https://doi.org/10.1145/2185520.2185543>

