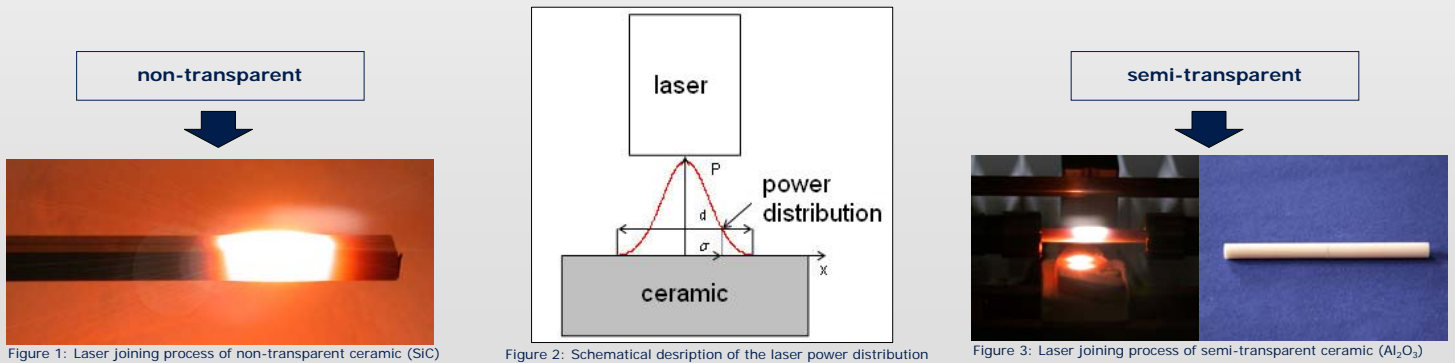


MATHEMATICAL MODELLING OF LASER JOINING PROCESSES

ABSTRACT

The aim of this work is essentially the mathematical modelling of the ceramic heating process by laser radiation. For these simulations the Finite-Element-Code COMSOL is used. The transient control of the laser beam is modelled by the implementation of additional dynamic equations in the code. The used heat transfer module of COMSOL offers two possibilities of modelling the interaction between laser beam and material. The first one is that the laser beam is regarded as an incoming thermal flow at the surface, at the other way basically the modelling of the laser beam as a local volume heat source is on focus. The results of the simulations, that have been achieved, show a good agreement between model and experiment, being an important part of further research works.

The **AIM** of the work, presented here, is to describe the laser joining process for ceramic materials. Particular the interaction of laser radiation with *non-transparent* and *semi-transparent* ceramics is on focus (in consideration of: scattering, reflection, absorption, ...).



Thermodynamical BASICS:

Fourier's differential equation

$$\delta_{is} * \rho(T) * C_p(T) * \frac{\partial T}{\partial t} = \text{div}(-k(T) * \text{grad}(T)) + Q$$

Radiation: Surface-to-ambient

$$-n * q = q_0 + h * (T_F - T_W) + \epsilon * \sigma * (T_{\text{Umgeb}}^4 - T^4)$$

Gaussian distribution of laser power

$$q = \frac{P_0}{2 * \pi * \sigma^2} * \exp(-0.5 * (\frac{x-x_0}{\sigma})^2 + (\frac{y-y_0}{\sigma})^2 + (\frac{z-z_0}{\sigma})^2)$$

Laser motion

$$x_0 = x_{00} + a * \cos(\omega * t) \quad y_0 = y_{00} + b * \sin(\omega * t)$$

On a plane surface: elliptical

$$x_0 = r_z * \cos(\omega * t) \quad y_0 = r_z * \sin(\omega * t) \quad z_0 = \text{const.}$$

On a curved surface: cylindrical

Exponential weakening of radiation

$$q_{\text{abs}}(\Delta d) = q_0 * \exp(-k_z * \Delta d)$$

Non-transparent ceramics

- laser radiation is absorbed on surface (penetration depth ca. 1 μm)
- energy transportation mainly due to thermal conductivity (SiC: ca. 100 W/(mK))
- no transmission, reflection depends on surface condition

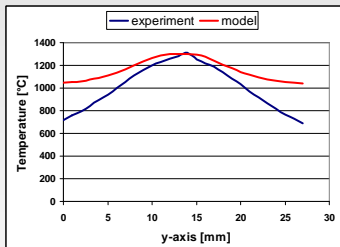


Figure 4: Temperature distribution on y-axis

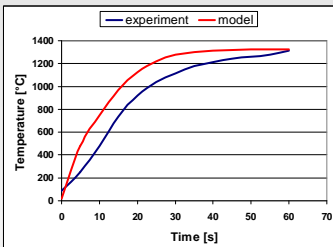
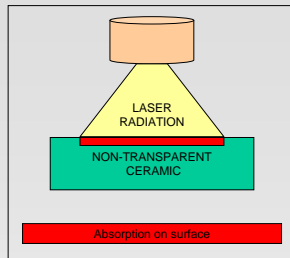


Figure 5: Heating rate of the sample

Semi-transparent ceramics

- laser radiation is absorbed in volume (laser radiation passes sample f(λ))
- energy transportation mainly due to laser radiation
- Thermal conductivity (Al₂O₃: ca. 36 W/(mK))
- high percentage of transmission, reflection depends on material properties

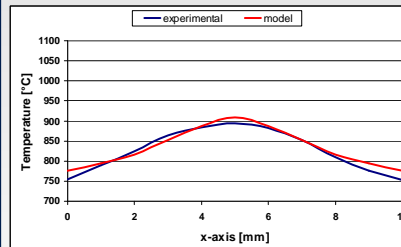


Figure 7: Temperature distribution on x-axis

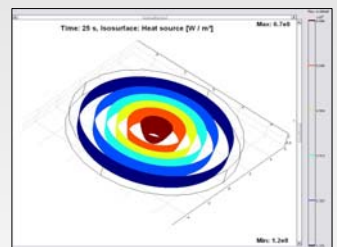
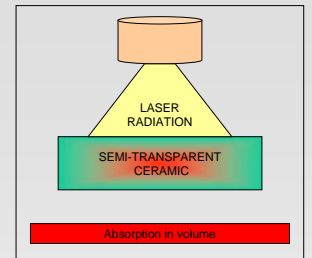


Figure 8: Weakening of heat source in volume

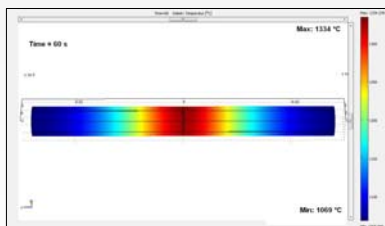


Figure 6: Calculated temperature field of SiSiC-sample

Description of experiment / model:

- rods SiSiC (l=28 mm, d=5.5 mm)
- laser beam power P₀ = 340 W
- laser motion on curved surface (cylindrical)
- time of joining process t = 60 s
- incoming laser radiation modeled as heat source [W/m³]
- no scattering in sample

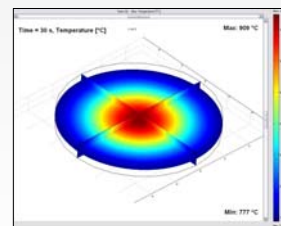


Figure 9: Calculated temperature field

Description of experiment / model:

- disc Al₂O₃ (h = 1 mm, d = 10 mm)
- laser beam power P₀ = 1.100 W
- time of process t = 30 s
- scattering in sample not considered
- absorbed laser radiation for heating:
 experiment: 1.29 % → 14.2 W in ceramic
 model: 1.30 % → 14.3 W in ceramic

CONCLUSIONS AND OUTLOOK

In order to gain conclusions about the obtained quality of the models of the laser joining process, the calculations are compared with experimental data. The results of the simulations, that have been achieved, show a good agreement between model and experiment. The development of a light scattering model is on focus for research work in order to gain the final aim: Modelling the complete laser joining process for ceramic materials (non-transparent and semi-transparent).

